

NATIONAL PETROLEUM RESERVE IN ALASKA

GEOLOGICAL REPORT

WALAKPA TEST WELL NO. 1

HUSKY OIL NPR OPERATIONS, INC.

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Edited by: R. G. Brockway

For the

U. S. GEOLOGICAL SURVEY

Office of the National Petroleum Reserve in Alaska

Department of the Interior

AUGUST 1983

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COMPOSITE LITHOLOGY LOG (In Pocket)

GEOLOGIC SUMMARY

INTRODUCTION

The Walakpa Test Well No. 1 is located in the SE 1/4, protracted Section 9, T20N, R19W, Umiat Meridian, approximately 15 miles south of Barrow, Alaska (see Figure 1 and 2). Drilling of the well commenced on December 25, 1979. The well reached a total depth of 3,666 feet on January 23, 1980. After testing a thin sandstone at approximately 2,075 feet, the well was plugged and abandoned and the rig released on February 8, 1980. Significant indications of hydrocarbons were restricted to approximately 15 net feet of Lower Cretaceous sandstone which tested gas at a calculated rate of 325,000 cubic feet per day.

PRE-DRILLING PROGNOSIS

The primary objective in drilling the Walakpa well was to evaluate the potential of an interpreted Upper Jurassic sandstone predicted to occur at approximately 2,075 feet. The objective horizon was seismically correlated with Jurassic sandstones in South Barrow No. 3 and was also thought to be correlative with the Jurassic Kingak sandstones penetrated in the South Simpson Test Well No. 1 and the Kugrua Test Well No. 1. The top of this sandstone was forecast at 2,075 feet measured depth. Oil and/or gas shows had been noted from this correlative sandstone in the above wells where porosities averaged approximately 16%. Seismic interpretation and isopach mapping of the Jurassic sandstone indicated truncation of the sandstone by the basal Cretaceous unconformity to the north of the Walakpa location. Seismic interpretations also indicated a phase reversal anomaly occurred to the south of the location. This phase reversal occurred in a south to north direction and was interpreted to be related to changes in fluid saturation from water-wet sandstone noted in the Kugrua and South Simpson wells to hydrocarbon saturated sandstone in the South Barrow area. Closure on the south and southwest was provided by regional dip.

Secondary objectives of the test were the Sag River Sandstone and sandstones of the Shublik Formation. The Shublik Formation was expected to directly overlie the argillite basement at this location. The top of the argillite was forecast at 3,550 feet measured depth.

Geochemical data in the area indicated potential source rocks in the Kingak Formation and overlying "Pebble Shale". Maturation studies indicated both oil and gas could be expected at the target objectives.

POST-DRILLING SUMMARY

The well penetrated the top of the argillite at a driller's depth of 3,633 feet and was drilled and cored to a total depth of 3,666 feet.

The primary objective sandstone was penetrated at a depth of 2,070-2,090 feet, or nearly as forecast. This sandstone is now informally referred to as the Walakpa sandstone. The entire sandstone was cored (No. 6). Core analysis indicated an average porosity through the 20-foot interval of approximately 18% and an average permeability of approximately 50 millidarcies. Average water saturation from core and log calculations are 50% and 40%, respectively. The zone was initially tested open hole but mechanical problems associated with this test resulted in the interval eventually being retested through perforations after running and cementing 7" casing. The well flowed dry gas at approximately 325 MCFPD on a 14/64" choke. Flowing tubing pressure was 260 psi with 1,026 psi FSIP. Additional details of the testing are in Appendix E. A special water-damage analysis performed on the core from this sandstone indicates fresh-water drilling fluid may have damaged the formation and resulted in lower flow rates (see Appendix G).

The age of the sandstone in the interval 2,070-2,090 feet is now considered to be Neocomian*. Current interpretation, as supported by more recent drilling and paleontological data, strongly indicates this Walakpa sandstone is approximately equivalent to other Lower Cretaceous sandstones such as the Kuparuk River.

No additional hydrocarbon reservoirs were noted in the well. The Sag River Sandstone and Shublik Formation sandstones did contain some porous intervals but all were interpreted to be water wet from log calculations.

More recent drilling in the area (Walakpa Test Well No. 2; Kuyanak Test Well No. 1) have served to better define the limits of the Walakpa sandstone. This data now indicates the unit pinches out depositionally to the north and that the southern productive limit lies somewhere between Walakpa No. 1 and the water-saturated sandstone present in Kuyanak No. 1. The potential lateral limits of this sandstone are still undetermined but appear to be large enough to provide a significant local source of gas.

* Biostratigraphic studies found Neocomian age foraminifera in the Walakpa sandstone of the Walakpa Well No. 2, drilled in early 1981.

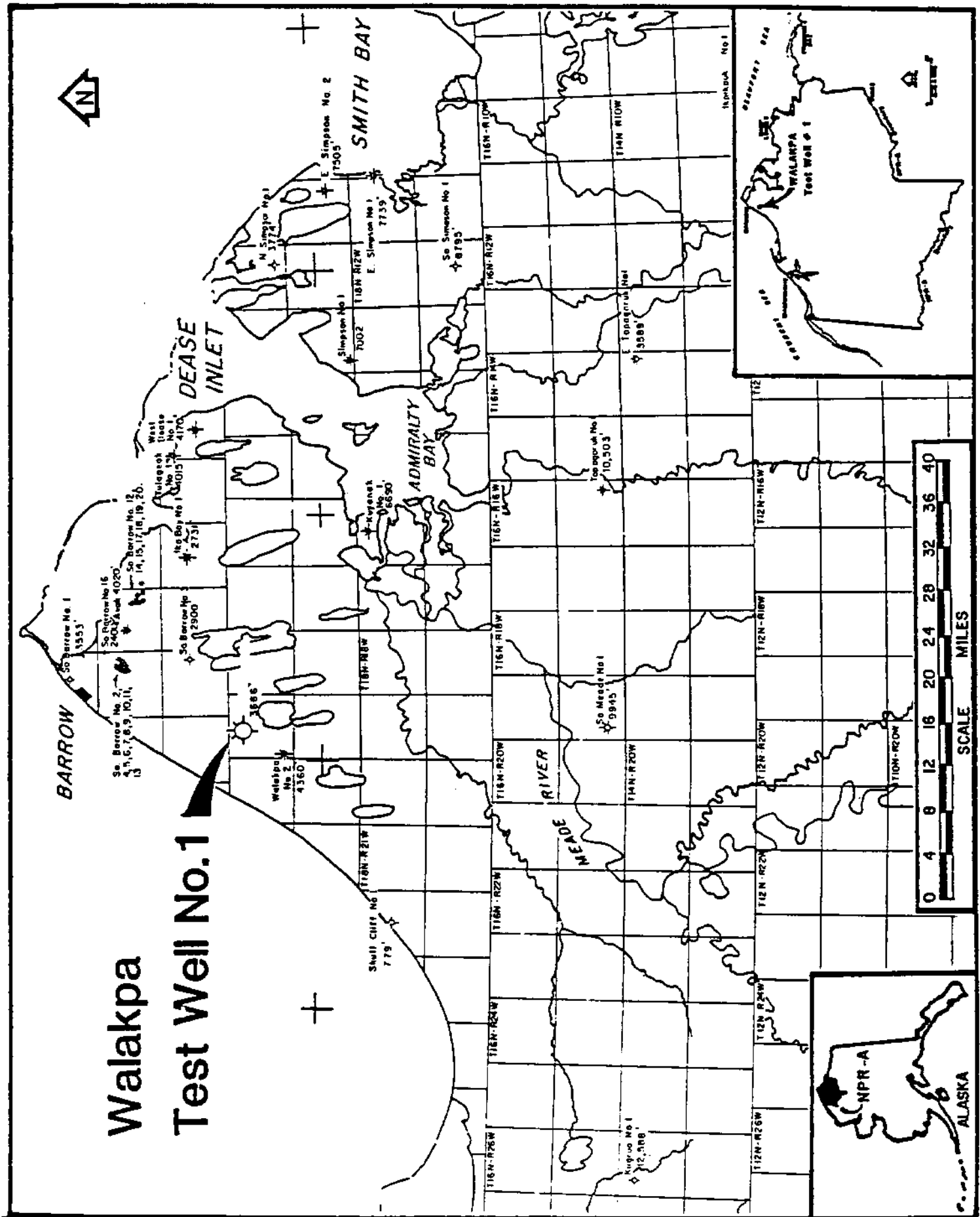
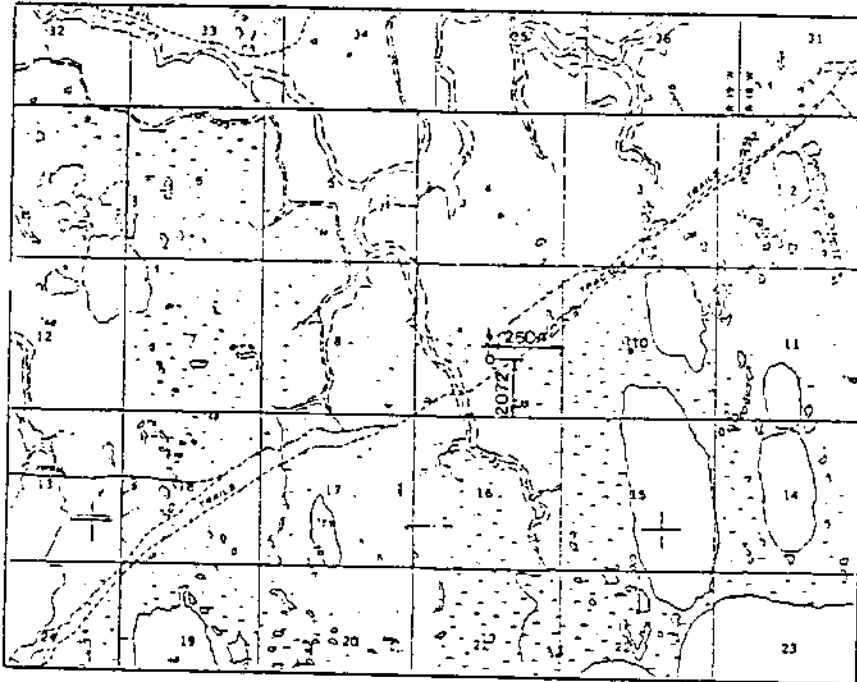


FIGURE 1 - LOCATION MAP - WALAKPA TEST WELL NO. 1



Computed location based on data from Barr Automated Surveys, Inc. to Husky Oil NPR Operations, Inc. dated Aug. 11, 1979, a copy of which is on file with Tectonics, Inc., Anchorage, AK.

WALAKPA 6-80
 LAT. = 71°05'57.63"
 LONG. = 156°53'03.79"
 Y = 6,253,083.18
 X = 632,366.26
 ZONE 6

CERTIFICATE OF SURVEYOR

I hereby certify that I am properly registered and licensed to practice land surveying in the State of Alaska and that this plat represents a location survey made by me or under my supervision, and that all dimensions and other details are correct.




AS STAKED
WALAKPA TEST WELL No.1
LOCATED IN
SE 1/4 PROTRACTED SEC. 9, T20N, R19W, UMIAT MERIDIAN, AK.
SURVEYED FOR
HUSKY OIL
N.P.R. OPERATIONS, INC.
 TECTONICS INC.
P.O. BOX 4-2265, ANCHORAGE, AK 99509

FIGURE 2 - SURVEYOR'S CERTIFICATE - WALAKPA TEST WELL NO. 1

WELLSITE GEOLOGIST'S REPORT

by
Gordon W. Legg

INTRODUCTION

The Walakpa Test Well No. 1 is located approximately 13 miles south-southwest of the South Barrow Gas Field and 8 miles southwest of the South Barrow Test Well No. 3, a dry hole with a total depth of 2,900 feet. The Walakpa well was drilled to test the so-called Simpson or Mid-Jurassic sandstone which is absent in the South Barrow Gas Field and is poorly developed and shaly in the South Barrow Test Well No. 3. Seismic interpretations indicated a possibility of a gas reservoir at the approximate expected level of the sandstone at Walakpa No. 1.

STRATIGRAPHY

WIRELINE TOPS

	<u>DRILLED DEPTH</u>	<u>SUBSEA DEPTH</u>
CRETACEOUS		
Torok Formation	100'	-50'
"Pebble Shale"	1701'	-1651'
Walakpa sandstone	2070'	-2020'
JURASSIC		
Kingak Formation	2087'	-2040'
TRIASSIC		
Sag River Sandstone	3224'	-3174'
Shublik Formation	3314'	-3264'
INDETERMINATE		
Argillite	3633'	-3583'

CRETACEOUS

Torok Formation: 100-1701'

The sediments of the Torok Formation for the most part are a sequence of clays and claystones with a few siltstones and sandstones down to 900' then has an increase in the thinly bedded siltstones and sandstones from 900' to 1701'. All of the sandstones are carbonaceous with flakes of black carbonaceous material and are extremely shaly and silty. They are very fine grained, and exhibit poor to very poor porosity, consequently must be considered as having very poor reservoir potential due to both low porosity and insufficient bed thickness. There is an observable gradational character from clays and claystones through siltstones to the very shaly, silty sandstones.

Only one minor show of oil in the ditch samples was observed in the Torok, occurring at 250'. A core was obtained just below this point at 257-287'. Of the 23' recovered, most was clay and claystone with three thin sandstones (1-2' thick) which were shaly and silty and exhibited no oil or gas shows.

Sediments from a depth of 390' to 900' are Early Cretaceous (Aptian-Albian) undifferentiated from paleontological (Foraminiferal) studies and from 900' to 1690' they are Early Cretaceous (Aptian-Early Albian). Paleontological studies based on palynology give ages of Early Cretaceous (Aptian-Albian) from 100' (conductor pipe) to 1690'. Electric logs revealed the top of the "Pebble Shale" (base of Aptian-Albian-top of Neocomian) at 1701', which is very close agreement with paleontological determinations.

"Pebble Shale": 1701-2070'

The dominant lithology of the "Pebble Shale" is a charcoal gray to black very organic shale. The shale contains "floating" rounded, clear, polished, greasy-appearing medium to coarse quartz grains. Occasionally, some of the grains are composed of chert. Toward the bottom of the formation and approaching the sandstone, the shale becomes highly carbonaceous, partly silty, and the color becomes more generally dark gray and gray-brown. Pyrite is common, and frequent large wood fragments were observed in Core No. 5 from 1981-2041'.

Ditch samples define the Neocomian "Pebble Shale" from 1690' to 2064' on the basis of foraminifera and from 1650' to 2064' on the basis of palynology. Both foraminifera and palynological determinations were able to define the base of the Neocomian at approximately 2064' by examining a core which was obtained from 2060' to 2120'. A more convenient marker would be that obtained at the base of the Walakpa sandstone which occurred at 2087' on the electric log. The zone from 2064' to 2080' appears to be a reworked zone, paleontologically, and it is impossible to assign a definite age to it. This is typical of so-called "unconformity sands" which, in this well, are most likely early Cretaceous in age, but contain some reworked Jurassic fossils.

Walakpa sandstone: 2071-2087'

The interval 2071-2087' is a sandstone with fair to good reservoir qualities. Some equivalent of this sandstone is present in most of the wells drilled in the National Petroleum Reserve and is variously known as the "Pebble Shale", "Unconformity sandstone", and "Kuparuk sandstone".

Lithologically, the sandstone is very fine to fine grained, carbonaceous, and glauconitic; occasional pyrite was observed. Two thin conglomerates are present in the upper 5' of Core No. 6 (2060-2120'). Both are composed of black chert and quartz pebbles and cobbles, large clay blebs and scattered to common glauconite pellets. One (2062.5-2063.25') has a very shaly matrix; the other (2064.5-2065.25') has a sandstone matrix with scattered hydrocarbon staining. Light oil staining was observed in the core from 2063.5' to 2080', accompanied by good petroleum odor and

varying degrees of fluorescence from dull gold to straw colored. Most of the shows yielded good cuts with a fair to good gold residue. Shows of gas were detected with the chromatograph. This sandstone was cored and then was tested both open hole and later through casing.

JURASSIC

Kingak Formation: 2087-3224'

The sediments representing the upper 963' of the Kingak Formation are alternating sequences of silty gray and brown shales with very argillaceous, light gray to gray-brown siltstones, and a few thin, rather argillaceous and silty sandstones. All sediments contain glauconite inclusions and pellets, and are somewhat carbonaceous. The shales are the dominant lithology above 2660' with the siltstones most prominent below this point.

At 3049' (electric log), a 55' Lower Barrow sandstone equivalent was entered. Fifty-three feet were recovered from a core at 3051' to 3111' (3058-3118' electric log). This sandstone, which is a gas producer in the Barrow gas fields, was fairly well developed in the Walakpa well but had marginal porosities in the range of 12-18% and did not contain hydrocarbon shows. The sandstone was generally light gray to brown, very fine to fine grained, carbonaceous and somewhat shaly and calcareous.

There were no shows of oil or gas in the Kingak and, with the exception of the Lower Barrow, none of the rock units had potential reservoir qualifications at this location.

From 3104' to 3224', the rocks are predominantly medium to light gray siltstones which grade downward to shales at the base. A few thin gray, very fine grained sandstones are present.

Rocks of Late to Early Jurassic are represented in the Walakpa No. 1 well. Foraminiferal and palynological determinations pick the top of the Late Jurassic at 2080' (2087' electric log). The base of the Late to Middle Jurassic is somewhat indistinct, but a depth of 3087' is chosen as a probable pick. A Late Triassic to Early Jurassic age has been assigned to the interval 3087-3360'. The electric log pick of 3224', which represents the top of the Sag River Sandstone, is preferred for the base of the Jurassic.

TRIASSIC

Sag River Sandstone: 3224-3314'

Rocks of the Sag River are primarily sandstones and siltstones with some thin shales and limestones. The sandstones are tan, medium gray and off-white, fine to very fine grained, glauconitic and have some carbonaceous material. They are siliceous and generally tight at the top of the interval but become increasingly calcareous with depth. No hydrocarbon shows were observed.

Interbedded with the sandstones are thin gray to dark gray, argillaceous and calcareous siltstones and gray to dark gray shales. Some reddish-brown shale was noted in the samples. Tan, microcrystalline, dolomitic limestone was observed in the 3230-3270' samples.

Although Anderson, Warren & Associates, Inc. do not pick a definite Triassic top in the Walakpa No. 1, the Sag River Sandstone has been given a Triassic age in other wells drilled in the National Petroleum Reserve in Alaska. For the purpose of this report, it is also placed in the Triassic.

Shublik Formation: 3220-3633'

The Shublik consists of limestones and generally calcareous sandstones, siltstones and shales. There is an alternating sequence of sediments of the above rock types which appear to be gradational with each other. These rocks are typically glauconitic, occasionally carbonaceous, and become increasingly fossiliferous with depth; most of the fossils are in limestones. Light gray, very fine to fine grained, calcareous, glauconitic sandstones and light to dark gray siltstones are the prominent lithology down to 3505'. Below this point, limestones become the major component, although sandstones and siltstones are common. The limestones vary in color from dark gray to white. Thin gray and gray-brown shales are scattered throughout the formation.

Foraminiferal determinations choose the zone from 3087' to 3360' as Late Triassic to Early Jurassic without committing a definite Triassic pick. Palynological determinations assigned the zone 3090' to 3360' as indeterminate. Foraminiferal determinations choose 3620' as the base of the Triassic while palynological determinations are more indistinct with definite Triassic extending only to 3420' followed by an apparent "data gap" from 3420-3545' and a final classification of indeterminate for rocks from 3545' to 3666'.

None of the rock units of the Triassic are considered to be a potential reservoir rock because they are generally quite well indurated and have low porosities. No shows of hydrocarbons were observed.

INDETERMINATE

Argillite: 3633-3666'

The low-grade metamorphics, which are collectively called argillite on the North Slope, were encountered at 3633' (electric log) and persisted to a total depth of 3666' (3672' electric log).

The argillite was charcoal gray in color and had a microgranular texture. It was micromicaceous, blocky, and dense. A core at 3656-3666' (Core No. 12) exhibited no apparent bedding, fissility, or schistosity.

OIL AND GAS SHOWS

All shows of oil and gas have been covered under the various stratigraphic headings; however, the gas show in the Walakpa sandstone at 2071-2087' (driller's depth) will be covered in greater detail.

Analysis of the cored interval 2062-2081' had porosities ranging from a low of 9.1% to a high of 25.1%. The average porosity value for the entire 19' interval was 18.2%. Permeabilities ranged from a low of 0.05 millidarcies to a high of 157 millidarcies, and with an average for the interval of 49 millidarcies. Oil saturations averaged around 3%, which is typical for a gas sand. Water saturations were also typical for gas sandstones with an average of around 50% (Appendix D).

Log calculations revealed an average porosity of approximately 21% and a water saturation of approximately 40% (these values compare favorably with core analysis).

Interpretation of the log calculations and core analysis would predict water-free gas production with some question about volume of production because of generally low permeability and probably low pressure due to the shallow depth.

An open-hole drill-stem test from 2063-2120' had gas-to-surface in 13 minutes, but freezing of water cushion and possibly hydrate water in the flow line precluded determinations of flow rates or pressures.

A decision was made to run 7" casing, cement, and perforate the Walakpa sandstone interval and place the zone on a 4-point production test. Perforations were made from 2071-2086', and the well was tested with varying choke sizes and with several flow periods. A flow of 325,000 CFGPD was obtained on a 14/64" choke with a flowing tubing pressure of 260 psi. Based on the flow rates, a calculated absolute open flow rate of 370,000 CFGPD was obtained.

CONCLUSION

The gas-producing sandstone (2071-2087') that was tested in Walakpa is considered only of fair reservoir quality on the bases of low to moderate permeability and porosity and limited reservoir thickness. The trapping mechanism is most likely controlled by updip pinchout of the sandstone to the north against the Barrow Arch. The producing limits of the sandstone could be quite extensive since it is almost certainly stratigraphically controlled.

The area in the vicinity of Walakpa could ultimately prove to be of interest as a future supply of gas for the village of Barrow.

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SUMMARY PERTINENT DATA, OPERATIONS & ANALYSIS*

WELL NAME: Walakpa Test Well No. 1

API NO.: 50-023-20013

OPERATOR: Husky Oil NPR Operations, Inc.

LOCATION: 2604' FEL, 2072' FSL
Protracted Section 9, T20N, R19W
Umiat Meridian
North Slope Borough, Alaska

COORDINATES: Latitude: 71°05'57.63" North
Longitude: 156°53'03.79" West
X = 632,366.26
Y = 6,253,083.18
Zone 6

ELEVATION: 50' Kelly Bushing; 31' Ground;
33' Pad

DATE SPURRED: December 25, 1979

TOTAL DEPTH: 3666' Driller; 3672' Wireline

DATE REACHED
TOTAL DEPTH: January 23, 1980

FORMATION AT
TOTAL DEPTH: Argillite

DATE RIG RELEASED: February 7, 1980

CASING: 13-3/8" @ 100'
9-5/8" @ 1786'
7" @ 3644'

SIGNIFICANT
HYDROCARBON SHOWS:

<u>Interval</u>	<u>Description</u>
2073-2088' (Perfs)	Tested 325 MCFD of dry gas

STATUS: Plugged and abandoned.

LOGGING RECORD:

Open Hole:	DIL/GR/SP	106-3666'
	BHCS/GR/TTI	106-3666'
	CNL/FDC/GR/CAL-0	106-3660'
	FDC/GR/CAL/RR	106-3660'
	HDT Dipmeter	106-1780' 1786-3655'
	HRT Temp.	200-3672'
	Mud Log	100-3666'
	Dc Exponent	700-3666'
	Velocity Survey	345-3670'
Cased Hole:	CBL/VDL/CR/CAL	1200-3567' 1700-2197'
Computed Logs:	Geogram Survey	100-3620'
	Saraband	1800-3660'

SIDEWALL CORES**

Run 1 1840-3615'; 30 shot, 25 recovered.

CONVENTIONAL CORES:

<u>No.</u>	<u>Interval</u>	<u>Recovery</u>	<u>Formation</u>
1	257- 287'	23'	Torok
2	1590-1613'	No recovery	Torok
3	1743-1760'	No recovery	"Pebble Shale"
4	1837-1897'	51'	"Pebble Shale"
5	1981-2041'	58'	"Pebble Shale"
6	2060-2120'	54'	Walakpa sandstone
7	2808-2825'	3.8'	Kingak
8	2930-2990'	60'	Kingak
9	2990-3020'	30'	Kingak
10	3051-3111'	60'	Sag River Sandstone
11	3360-3420'	60'	Shublik
12	3656-3666'	10'	Argillite

CORE ANALYSIS:

<u>Date</u>	<u>Interval</u>	<u>Core No.</u>	<u>Sample Nos.</u>
1-14-80	2062-2081'	6	1-20
1-14-80	3051-3096'	10	21-66

TESTS (DRILL-STEM TESTS):

<u>No.</u>	<u>Interval</u>	<u>Summary Description</u>
1	2063-2120'	Open-hole drill-stem test, gas to surface in 13 minutes, flow line froze, test aborted.
2	2073-2088'	Perforated 7" casing, four shots/foot, well flowed dry gas at approximately 325 MCFGPD.

FLUID ANALYSIS:

<u>Source</u>	<u>Type Analysis</u>
Drill-Stem Test No. 1	Gas and recovery fluid analysis (see Appendix F).
Drill-Stem Test No. 2	Gas, drill fluid, water cushion and sample-chamber fluid (see Appendix F).

SPECIAL ANALYSIS: Fresh-water susceptibility analysis interval 2066-2078' (Core No. 6) (see Appendix G).

Miscellaneous Pertinent Data

WELLSITE GEOLOGIST: G. Legg
W. D. Fenex

DRILLING CONTRACTOR: Brinkerhoff Signal, Inc., Rig 31

MUDLOGGERS: The Analysts

BIOSTRATIGRAPHIC ANALYSIS: Anderson, Warren & Associates, Inc.

- * Copies and/or reproducibles of all geological data are available from:

National Oceanic and Atmospheric Administration
EDIS/NGSDC (D62)
325 Broadway
Boulder, CO 80303
- ** Sidewall cores were utilized for various analyses including: lithology, paleontology, and geochemistry.

WALAKPA NO. 1
 DRILL CUTTINGS AND CORE DESCRIPTION
 BY

G. LEGG - 100-1800'
 - 3051-3666'
 D. FENEX - 1800-3051'

NOTE: Sample descriptions and depths are from wellsite and are not adjusted to mechanical control.

DRILLED DEPTH
 (FEET BELOW
 KELLY BUSHING)

0 - 100	No samples caught.
100 - 140	Clay: gray, soft, sticky to gummy with occasional very fine grained flecks of carbonaceous material.
140 - 200	Clay: as above, with trace of Sandstone: gray, fine grained, carbonaceous flakes.
200 - 240	Clay: as above, with increase in silt to very fine grained sand particles and with 10% carbonaceous flecks.
240 - 257	Clay: as above, with Sandstone: gray, very silty, heavy clay matrix; very fine grained to silt, some carbonaceous flecks, bright yellow fluorescence in part, very slow cut, nonstreaming.
257 - 287	<u>Core No. 1: Cut 30', Recovered 23'</u>
257.0-258.0' (1.0')	Clay and Claystone: medium gray, soft to poorly indurated, gummy to sticky, noncalcareous, nonswelling.
258.0-258.5' (0.5')	Sandstone: medium gray, very argillaceous and silty, grading to siltstone and clay, very fine grained to silt, soft to friable with heavy clay matrix, poor to nil porosity, grading to silty clay toward bottom.
258.5-268.0' (9.5')	Clay and Claystone: as above, but slightly silty and very slightly micromicaceous in part, varying between micromicaceous and silty to sandy to nonmicaceous and nonsandy.

268.0-269.0' (1.0')	Sandstone: medium gray, very argillaceous as above, no show.
269.0-274.5' (5.5')	Claystone: as above.
274.5-275.0' (0.5')	Sandstone: as above, but even more clayey, completely gradational with claystone.
275.0-278.0' (3.0')	Claystone: as above.
278.0-278.2' (0.2')	Sandstone: mostly as above, but slightly more porous, some evidence of very slight permeability, no show.
278.2-280.0' (1.8')	Claystone: as above.
280.0-287.0' (7.0')	No recovery.
287 - 380	Clay and Claystone: as in Core No. 1.
380 - 410	Clay: as above, but with increase in floating sand and silt grains.
410 - 650	Clay: as above, but with rare sand to silt grains.
650 - 770	Clay: as above, with trace of Sandstone: gray, very fine grained to silt, very argillaceous with heavy clay cement, some very fine grained carbonaceous material, poor porosity, no show.
770 - 950	Clay: as above, with minor Sandstone: gray to brown, very fine grained to silt, argillaceous, poor to moderately indurated, poor porosity, no show.
950 - 1070	Clay: as above, with trace to 10% Sandstone: gray, silty, clay matrix, poor porosity.
1070 - 1100	Clay: as above, with Sandstone and Siltstone: white to gray, very fine grained to silt, some very thin carbonaceous flakes, very argillaceous, grading to clay, some poor to fair porosity, some bright yellow fluorescence, very slight to nil cut from gel-like emulsion, possible free oil, probably contamination.
1100 - 1160	Clay: as above, with Sandstone and Siltstone: as above, but no fluorescence.

- 1160 - 1250 Clay: very silty to sandy with sandstone becoming mostly siltstone.
- 1250 - 1460 Clay: becoming very silty, nearly unconsolidated, becoming a very clayey siltstone, with Sandstone: dark gray to brown, very silty, essentially siltstone, poor porosity, no show.
- 1460 - 1490 Clay: mostly as above, but with large increase in silt and very fine grained sand residue when clay is washed out, with Siltstone: dirty gray, sandy, very argillaceous, carbonaceous.
- 1490 - 1520 Clay: as above, with Siltstone: as above with abundant free pyrite.
- 1520 - 1550 Sample contaminated with diesel oil from unknown source.
- 1550 - 1580 Clay: as above, with Siltstone and Sandstone: light gray to off white, very fine grained to silt, extremely carbonaceous with flakes and inclusions, poor porosity, no show, with rounded black chert pebbles and one rounded smoky quartz pebble.
- 1580 - 1590 Clay, Siltstone, and Sandstone: as above, but no pebbles.
- 1590 - 1613 Core No. 2: Cut 23', No recovery.
- 1613 - 1700 Clay: as above, with Siltstone: dirty gray, very argillaceous, grading to silty claystone with Sandstone: gray, very fine grained to silt, some fine grained, abundant feldspar grains, very argillaceous, grading to siltstone and claystone, poor porosity, no show.
- 1700 - 1730 Shale: dark gray, very organic and carbonaceous, subfissile to fissile, poor to moderately indurated, with Clay and Siltstone: as above.
- 1730 - 1743 Shale: as above, with occasional free rounded, clear, coarse grained quartz and some broken pebbles of quartz and gray chert.
- 1743 - 1760 Core No. 3: Cut 17', No recovery.
- 1760 - 1790 Shale: as above, but becoming more light gray, very silty, occasionally grading to siltstone; less organic.
- 1790 - 1800 Shale: as above, with occasional rounded grains as above.
- 1800 - 1837 Shale: as above.

1837 - 1897

Core No. 4: Cut 60', Recovered 51'

- 1837.0-1859.5'
(22.5') Shale: black to dark gray, subfissile, micromicaceous, rare pyrite inclusions, rare floating quartz pebbles, well rounded; minute carbonaceous inclusions.
- 1859.5-1860.0'
(0.5') Siltstone: medium dark gray, very argillaceous, sandy in part (floating well rounded, medium grained quartz), minutely micaceous, common carbonaceous debris, very slightly calcareous, well indurated.
- 1860.0-1861.0'
(1.0') Shale: as above.
- 1861.0-1861.5'
(0.5') Siltstone: as above.
- 1861.5-1864.0'
(2.5') Shale: as above.
- 1864.0-1864.75'
(0.75') Marlstone (Concretion?): medium gray brown, smooth, very well indurated, with coarse calcite-filled veins and pelecypod(?) cast; some minute carbonaceous inclusions.
- 1864.75-1888.0'
(23.25') Shale: as above, with pyrite nodules, rare rounded quartz pebbles, rare wood fragments, carbonized, and grading to coal, black and shiny, partially replaced by pyrite, rare microfossils and spicules; rare fossil prisms.
- 1888.0-1897.0'
(9.0') Not recovered.

1897 - 1945

Shale: as above.

1945 - 1981

Probably Sandstone as interpreted by drilling time; only minor amounts of unconsolidated quartz grains, very fine to fine grained, clear, with loose pyrite, subrounded to subangular, well to fair sorted, occur in the largely Shale sample.

1981 - 2041

Core No. 5: Cut 60', Recovered 58'

- 1981.0-2030.0'
(49.0') Shale: dark gray-brown, subfissile to fissile, coarsely micaceous grading to micromicaceous towards base with scattered rounded quartz pebbles, pyrite inclusions, scattered large wood fragments, carbonaceous, grading to black, shiny coal (pyrite replacement occurs in part); abundant spicules filled with olive-green clay; occasional microfossils; generally silty to very silty; carbonaceous debris.
- 2030.0-2031.0'
(1.0') Siltstone: medium gray brown, argillaceous, abundant carbonaceous debris and fine tan fossil debris.
- 2031.0-2039.0'
(8.0') Shale: as above, with some pyritized worm tubes.
- 2039.0-2041.0'
(2.0') No recovery.

2041 - 2060

Essentially Shale: as above.

2060 - 2120

Core No. 6: Cut 60', Recovered 54'

- 2060.0-2061.5'
(1.5') Shale: dark gray brown, as above.
- 2061.5-2062.5'
(1.0') Shale: as above, becomes very conglomeratic with large floating black subrounded chert and quartz cobbles and pebbles; abundant quartz grains, varying from fine to coarse grained, very poorly sorted; largely dark brown clay matrix, becomes sandier towards base; large wood fragment.
- 2062.5-2063.25'
(0.75') Conglomerate: very shaly matrix with cobbles and pebbles, as above; some large clay blebs; scattered bright green glauconite pellets.
- 2063.25-2064.5'
(1.25') Sandstone: light gray brown, "salt and pepper", fine to medium grained, subrounded and subangular, fair sorting, moderately indurated, slightly calcareous (appears to be siderite cement), common bright green

- glaucanite pellets, some milk-white tripolitic chert, poor to fair intergranular porosity, light oil stain, good petroleum odor, varying degree of fluorescence from dull gold to straw, light straw milky cut, leaves gold residual cut on spot plate.
- 2064.5-2065.25'
(0.75') Conglomerate: dark gray brown, composed of large rounded pebble- to cobble-sized quartz and black, smoky gray chert, rare dark gray rounded clay blebs, rare milk-white tripolitic chert, some fossil debris and plant remains, in a matrix of Sandstone: as above, common green glauconite pellets, siderite cement, petroleum odor, scattered stain, dull gold fluorescence, slow cut leaving a residual cut on spot plate; generally poor intergranular porosity.
- 2065.25-2068.25'
(3.0') Sandstone: as above, with generally better porosity, dull to bright gold fluorescence, slow blossoming cut, well cemented with siderite.
- 2068.25-2068.75'
(0.5') Sandstone: as above, very fine to fine grained, very poor porosity; no odor, stain, cut, or fluorescence.
- 2068.75-2079.5'
(10.75') Sandstone: as above at 2068.25', with show as above, general increase in porosity.
- 2079.5-2080.0'
(0.5') Sandstone: as above, with abundant pebbles and cobbles, some white tripolitic chert and carbonized plant remains; vertical fractures.
- 2080.0-2080.5'
(0.5') Sandstone: as above, very silty, hard and tight, argillaceous, black-brown clay cement; no odor, stain, cut, or fluorescence.
- 2080.5-2086.0'
(5.5') Shale: dark gray-brown, very silty, grades to siltstone in part, some spicules, becomes shalier towards base.
- 2086.0-2092.0'
(6.0') Siltstone: dark gray-brown, argillaceous, micromicaceous, with coarse green glauconite pellets.

2092.0-2100.0' (8.0')	Interbedded Shale: dark brown, smooth, subfissile, micromicaceous, slightly silty, some clay-filled spicules and Siltstone: as above.
2100.0-2113.0' (13.0')	Shale: as above, with spicules and pyritized worm burrows, some carbonized wood debris, rare microfossils.
2113.0-2114.0' (1.0')	Siltstone: as above.
2114.0-2120.0' (6.0')	Not recovered.
2120 - 2172	Shale: as above, grades to siltstone in part, with large green glauconite pellets.
2172 - 2178	Sandstone: unconsolidated, composed of quartz grains, coarse, subrounded. (Interpretation based mainly upon drilling time.)
2178 - 2194	Shale: as above.
2194 - 2200	Sandstone: as above, unconsolidated.
2200 - 2335	Claystone: brown, lumpy, moderate to poorly indurated, with coarse glauconite pellets, pyrite inclusions, some pyritized worm tubes; rare ironstone concretions, tan, hard, brittle.
2335 - 2465	Siltstone: light gray, clean, moderately indurated, with minute green glauconite pellets, very slightly calcareous, grades to sandstone, composed of unconsolidated quartz grains, with some loose pyrite and glauconite, from 2345-2352'; trace fossil prisms.
2465 - 2550	Alternating Shale and Siltstone: as above, with some concretions.
2550 - 2570	Shale: light medium gray, very minutely micaceous, smooth to silty in part; some minute carbonaceous material, blocky.
2570 - 2580	Siltstone: as above, argillaceous, some loose rounded quartz grains.
2580 - 2655	Shale: gray, as above, with abundant bentonite streaks, minute carbonaceous debris, some pyrite inclusions, silty in part.

- 2655 - 2745 Siltstone: light gray to tan, clean, blocky, well indurated, rare minute glauconite pellets, becomes sandy in part, noncalcareous, grades to very argillaceous in part; with interbedded Shale: gray, as above, some pyrite inclusions.
- 2745 - 2767 Siltstone: light gray, sandy in part, grades to sandstone in part, clean, noncalcareous, moderately indurated, grades to gray siltstone, argillaceous in part, with some concretions, as above.
- 2767 - 2775 Shale: light medium gray, as above.
- 2775 - 2790 Siltstone: as above, very argillaceous.
- 2790 - 2808 Shale: as above.
- 2808 - 2825 Core No. 7: Cut 17', Recovered 3.8'
- 2808.0-2811.8' (3.8') Siltstone: medium to light gray-brown, very argillaceous, sandy in part, grades to shale in part, micromicaceous, abundant coarse carbonaceous debris, moderately indurated.
- 2811.8-2825.0' (13.2') No recovery.
- 2825 - 2880 Siltstone: as above, becomes slightly "salt and pepper", abundant coarse carbonaceous debris, micaceous, rare glauconite pellets, with thin interbedded shale, as above.
- 2880 - 2930 Shale: medium gray-brown, subfissile, micromicaceous, some minute carbonaceous debris, very bentonitic, some fossil fragments, pyrite inclusions.
- 2930 - 2990 Core No. 8: Cut 60', Recovered 60'
- 2930.0-2958.0' (28.0') Shale: medium gray-brown, subfissile, micromicaceous, minute carbonaceous debris, moderately well indurated, noncalcareous, with abundant blebs of bentonite, scattered rare worm tubes replaced by pyrite, rare concretions and spicules filled with gray clay; rare large wood fragments, coalified; and with one small intact pelecypod replaced by pyrite.
- 2958.0-2966.0' (8.0') Shale: as above, becomes very silty, grades to siltstone, with pyritized worm tubes.

	2966.0-2972.0' (6.0')	Shale: as above.
	2972.0-2988.0' (16.0')	Siltstone: gray-brown, very argillaceous, well indurated, common carbonaceous debris, micromicaceous, rare green glauconite pellets, noncalcareous.
	2988.0-2990.0' (2.0')	Siltstone: as above, grades to sandstone in part.
2990 - 3020	<u>Core No. 9: Cut 30', Recovered 30'</u>	
	2990.0-3020.0' (30.0')	Siltstone: dark gray-brown, very argillaceous, sandy, micromicaceous, common carbonaceous debris and green glauconite pellets, bioturbated, thinly laminated, rare bentonite blebs; grades to light gray Sandstone clasts; occasional wood fragments, no porosity, no shows.
3020 - 3042	Siltstone: as above.	
3042 - 3051	Sandstone: light gray brown, very fine to fine grained, subrounded and subangular, well sorted, clean, slightly "salt and pepper", calcareous, poor to fair intergranular porosity; no odor, stain, cut, or fluorescence.	
3051 - 3111	<u>Core No. 10: Cut 60', Recovered 60'</u>	
	3051.0-3056.0' (5.0')	Sandstone: light to medium gray, very fine grained to silt, grading to siltstone, slightly bioturbated with marbling of darker gray argillaceous material, occasionally finely micaceous, and with rare fragments of partly carbonized wood, occasionally pyritized, very slightly carbonaceous, well cemented with silica and clay, moderate to well indurated, generally poor to nil porosity, occasional thin lenses of poor to fair porosity, no show; some rare snow white talc-like mineral on occasional closed fracture, probably kaolin; sandstone appears to be very well indurated and silicified in vicinity of fracture.
	3056.0-3065.0' (9.0')	Sandstone: light gray to tan, very fine grained to fine grained, slightly

- less argillaceous and bioturbated than above, occasionally slightly friable to moderately indurated, very slightly calcareous, poor to fair porosity, no show.
- 3065.0-3066.0'
(1.0') Sandstone: light to medium gray, very fine grained to silt, argillaceous, well indurated, very slightly calcareous, poor to nil porosity, no show.
- 3066.0-3069.0'
(3.0') Sandstone: light gray to tan, very fine grained to fine grained as interval 3056.0' to 3065.0' above.
- 3069.0-3076.0'
(7.0') Sandstone: light to medium gray, very fine grained to silt, argillaceous, with occasional very finely micaceous argillaceous material, very slightly calcareous as above, generally poor porosity, occasional thin zones of poor to fair porosity, no show.
- 3076.0-3098.0'
(22.0') Sandstone: light to medium gray, very fine grained to silt, with some fine grained, varies between moderate to well indurated and moderate to well cemented, very slightly calcareous as above; porosity varies from poor to nil to poor to fair, no show; generally more silty and argillaceous than above, becoming more argillaceous and slightly carbonaceous below 3086', with occasional thin very finely micaceous and carbonaceous shale partings; one large wood fragment approximately 3-4 centimeters in diameter at 3093', high specific gravity, very heavily pyritized, but with original wood texture and grain.
- 3098.0-3100.0'
(2.0') Sandstone: light to medium gray, as above, very fine grained to silt, very slightly calcareous, argillaceous and slightly carbonaceous, but with occasional grains of green glauconite, poor to nil porosity.
- 3100.0-3109.0'
(9.0') Siltstone: gray to dark gray, argillaceous and sandy, grading to

- very silty sandstone; carbonaceous, very slightly calcareous, moderate to well indurated.
- 3109.0-3111.0'
(2.0') Siltstone: as above, but slightly more sandy, and with occasional lenses and partially rounded inclusions of spar calcite, appears to be detrital, but probably is replacement (no recognizable fossil form).
- 3111 - 3120 Shale: medium gray, grading to siltstone, calcareous, with Siltstone: gray, very argillaceous, grading to shale.
- 3120 - 3140 Siltstone: as above, grades in part to very silty sandstone, gray, argillaceous, very fine grained, well indurated, poor to nil porosity.
- 3140 - 3160 Siltstone: as above, but becoming more sandy, grading to sandstone, with Sandstone: mostly as above, but with some finely disseminated glauconite and with minor Shale: as above.
- 3160 - 3170 Siltstone: as above, with minor Sandstone: light gray, very fine to fine grained, black carbonaceous and coal flakes, very slightly calcareous, siliceous, very well indurated.
- 3170 - 3190 Siltstone: light gray, very argillaceous and sandy, very carbonaceous, with very fine grained coal flakes with Sandstone: white to light gray, mottled with black carbonaceous flakes, very fine grained to silt, grades to siltstone, very slightly calcareous, siliceous cement, very well indurated, with minor Shale: as above.
- 3190 - 3210 Siltstone and Sandstone: as above, with Shale: as above and with some Shale: red brown, very finely micaceous in part, poor to moderately indurated.
- 3210 - 3220 Sandstone: tan to pale gray; mostly fine grained, mottled with black carbonaceous material and shale particles, occasional glauconite, dense, tight and siliceous, some friable with fair porosity, no show, with Shale: as above, with minor Siltstone: as above.
- 3220 - 3230 Shale: as above, with some Shale: dark gray to black, very organic and carbonaceous, earthy, with Sandstone and Siltstone: as above.

- 3230 - 3240 Shale and Sandstone: as above, with Limestone: very dolomitic or sideritic, tan, occasionally earthy, microcrystalline, well indurated, occasional inclusions of sand and glauconite pellets.
- 3240 - 3250 Shale and Sandstone: as above, with Limestone: as above, but becoming very silty in part, grading to siltstone, with Siltstone: gray, very calcareous, argillaceous, well indurated.
- 3250 - 3260 Sandstone: gray to off white, very fine grained to fine grained, very silty, grading to Siltstone: argillaceous, occasional black carbonaceous flakes, occasional glauconite grains and pellets, moderate to well indurated, poor porosity, no show, with Siltstone, Shale and Limestone: as above.
- 3260 - 3270 Sandstone: as above, but becoming more calcareous, grading in part to limestone.
- 3270 - 3280 Sandstone: as above, with heavy calcareous matrix and occasional white clay in matrix.
- 3280 - 3290 Sandstone: as above, with Siltstone: gray to dark gray, very sandy, occasional glauconite and carbonaceous particles, and with trace of Shale: pale gray, waxy, nearly claystone.
- 3290 - 3310 Shale: as above, with Shale: dark gray to black, organic, earthy, occasional floating rounded quartz grains, with Siltstone and Sandstone: as above.
- 3310 - 3320 Shale: as above, but becoming more silty, grading to siltstone, occasional glauconite pellets, with sandstone, becoming more silty - grading to siltstone, and with Siltstone: grading to shale, occasional glauconite pellets.
- 3320 - 3330 Siltstone and Sandstone: gradational, frequent pellets and inclusions of glauconite, with Shale: as above, and with some limonite and limonitic clay, rust-brown with occasional oolites and trace of Limestone: tan to brown, microcrystalline, dense.
- 3330 - 3340 Siltstone and Sandstone: as above, becoming well indurated, with Shale: as above, with increase in limonite, and with trace of Limestone: as above.
- 3340 - 3350 Siltstone and Sandstone: as above, grading in part to limestone, with increase in Limestone: some dark gray, white to tan in part, fossil pelecypod shells, occasional glauconite, frequently silty, with Shale: as above.

3350 - 3360 Predominantly Shale: pale gray, smooth, fissile, micromicaceous, very fine carbonaceous flakes, rare glauconite pellets, with Limestone: as above, and with minor Siltstone and Sandstone: as above.

3360 - 3420 Core No. 11: Cut 60', Recovered 60'

3360.0-3372.0' (12.0') Siltstone: very sandy, argillaceous and calcareous, grading to silty sandy Limestone: gray to gray-brown, mostly silt with some very fine grained sand zones, very heavy calcareous matrix, very well indurated and dense, occasional zones of pelecypod accumulations, occasional glauconite grains, poor to nil porosity, grading from essentially sandstone at top to siltstone and then to limestone near bottom.

3372.0-3375.0' (3.0') Limestone: gray and gray-brown, very argillaceous, silty and occasionally sandy, grading to very calcareous siltstone.

3375.0-3377.0' (2.0') Siltstone: as above.

3377.0-3393.0' (16.0') Sandstone: gray to gray-brown, very silty, grading in part to siltstone, very argillaceous and calcareous, very fine grained, occasional glauconite, poor to nil porosity; very shaly in bottom one foot.

3393.0-3396.0' (3.0') Shale: gray, smooth, micromicaceous, fissile, carbonaceous flakes, noncalcareous except for occasional fossil pods.

3396.0-3419.5' (23.5') Siltstone: as above, but increase in glauconite, and with occasional carbonaceous inclusions; dark green translucent mineral 3405-3410', waxy, soft, appears to be chlorite; no glauconite or chlorite below 3410', but occasional pyrite.

3419.5-3420.0' (0.5') Shale: pale gray, noncalcareous, as above.

- 3420 - 3430 Shale: as in Core No. 11, with Siltstone: as in Core No. 11.
- 3430 - 3460 Sandstone: off white to light gray, mottled green with abundant glauconite pellets and grains, very fine grained, very calcareous with heavy matrix, argillaceous and silty, poor porosity, no show, with Shale and Siltstone: as above.
- 3460 - 3470 Sandstone: as above, occasional calcite replaced pelecypods.
- 3470 - 3480 Sandstone: becoming very fine grained to fine grained, friable in part, heavy clay and calcite matrix, poor porosity, no show.
- 3480 - 3490 Sandstone: as above, but more firmly indurated, with Siltstone: dark gray, sandy, very calcareous, with inclusions of yellow-brown limonitic claystone, frequent loose coarse grained rounded quartz, abundant pelecypod fragments.
- 3490 - 3510 Sandstone and Siltstone: as above, becoming more calcareous, grading to limestone, with Shale: brown, micromicaceous, subfissile to fissile.
- 3510 - 3530 Limestone: dark gray to brown, very silty and sandy, grading to siltstone and sandstone, very well indurated, occasional glauconite, occasional pelecypod fragments, with Sandstone and Siltstone: as above.
- 3530 - 3560 Limestone: as above, but becoming more dense, appears to be siliceous, with some Sandstone and Siltstone: as above.
- 3560 - 3570 Limestone: becoming more sandy, grading to Sandstone and Siltstone: as above.
- 3570 - 3590 Limestone: as above, with some Limestone: white, soft, very chalky, with Shale: gray and gray-brown, smooth, fissile, with Sandstone and Siltstone: as above.
- 3590 - 3600 Limestone: white to light tan, very chalky, abundant fossil fragments, soft to very well indurated, nil porosity, no show, with minor Shale, Siltstone and Sandstone: as above.
- 3600 - 3610 Limestone: as above, but becoming sandy in part, with sand grains and very fine grained inclusions of black mineral, could possibly be argillite, dense, with minor Sandstone: very calcareous, and minor Shale: as above.

3610 - 3620 Limestone: as above, but becoming even more silty, sandy, grading to sandstone, and with increase in very fine grained black inclusions.

3620 - 3656 Argillite: charcoal gray, microgranular texture, micromicaceous, blocky, dense.

3656 - 3666 Core No. 12: Cut 10', Recovered 10'

3656.0-3666.0' Argillite: charcoal gray,
(10.0') microgranular, micromicaceous, with scattered mica; breaks at 30° and 60° with slate-like cleavage, occasional hairline discontinuous lenses filled with calcite (seldom exceeding 1-2 centimeters and with random orientation).



HUSKY OIL NPR OPERATIONS, INC.
U.S. GEOLOGICAL SURVEY ONPRA

LOGGING REPORT

WELL NAME WALAKPA #1

Date December 30, 1979 Driller Depth 1800'

Elevation 50' KB - 31' GL Logger Depth 1799'

Logs Run and Intervals

DIL/GR/SP	106-1793'
BHCS/GR (Caliper failed)	106-1788'
FDC/CNL/GR/CAL	106-1790'
HDT Dipmeter	106-1780'

Additional Logs to Run

Zones of Interest

Depth	Gross Thickness	Net Feet of Porosity	Lith	Porosity	Probable Fluid Content
NO ZONES OF INTEREST					

Discussion:

Schlumberger TD: 1799' Csg: 106' (13 3/8")
Driller TD: 1800'

Log Tops & Correlations:

Top - Pebble Shale: 1701' (-1651') = 6472' (-6412') on So. Meade - 4761' high.

Geological Correlation Plans:

NONE

DAVE FENEX

Wellsite Geologist

Log Analyst



LOGGING REPORT

WELL NAME WALAKPA #1

Date January 24, 1980 Driller Depth 3666'

Elevation 50' KB - 31' GL Logger Depth 3672'

Logs Run and Intervals

HRT Temp Log (#1)	200-3672'
DIL/GR/SP	1786-3666'
BHCS/GR	1786-3660'
FDC/CNL/GR/CAL	1786-3660'
HOT Dipmeter	1786-3655'
Velocity Survey	345-3670'
HRT Temp Log (#2)	200-3672'
CST Sidewall Cores, shot 30, recovered 25	

Zones of Interest

Depth	Gross Thickness	Net Feet of Porosity	Lith	Porosity	Probable Fluid Content
2071-2087'	16'	16'	SS	22%	Gas

Discussion:

SS @ 2071-2086', net pay 16', aver. density porosity 22.5%, aver. neutron porosity 22.0%, max. porosity 25%, minimum porosity 18%, Sw estimate @ 40-50%.

Log Tops & Correlations:

"Basal Cret" SS @ 2071'
 Sag River? @ 3224'
 Shublik @ 3264'
 Argillite @ 3631'

Well Completion

Cased hole DST after running 7" casing.

G. Legg

Geologist

Geologist

CORE LABORATORIES, INC.
Petroleum Reservoir Engineering
 DALLAS, TEXAS

U.S. GEOLOGICAL SURVEY
 HUSKY OIL CO., NPR OPERATOR
 WILAKFA #1
 NORTH SLOPE, ALASKA

DATE : 14-JAN-80
 FORMATION :
 DRLG. FLUID: WBM
 LOCATION : BOYLES LAW POROSITY

FILE NO : BP-3-563
 ANALYSTS : WSP, TLS
 LABORATORY: ANCHORAGE

CORE ANALYSIS RESULTS

SAMPLE NUMBER	DEPTH FEET	PERMEABILITY (MD)		POR %	GRAIN DEN.	FLUID SATS.		DESCRIPTION
		MAXIMUM	90 DEG VERTICAL			OIL	WTR	
1	2062.0	0.84		9.7	2.64	6.4	51.4	ssif-carb carb
2	2063.0	6.46		12.7	2.67	0.0	22.0	ssivf-fgr
3	2064.0	83.		17.2	2.66	0.0	50.8	same
4	2065.0	123.		22.0	2.66	0.5	51.9	same
5	2066.0	68.		21.3	2.66	1.1	52.4	same
6	2067.0	10.		17.3	2.67	4.1	49.8	same
7	2068.0	0.11		9.1	2.73	0.0	72.4	same
8	2069.0	92.		21.2	2.66	4.9	56.6	same
9	2070.0	31.		20.1	2.66	0.6	61.9	same
10	2071.0	38.		20.3	2.66	5.1	59.9	same
11	2072.0	55.		20.8	2.67	3.5	51.7	same
12	2073.0	43.		20.3	2.66	1.1	55.0	same
13	2074.0	25.		19.9	2.78	2.9	44.5	same
14	2075.0	157.		25.1	2.68	3.5	52.3	same
15	2076.0	95.		22.5	2.67	3.8	45.2	same
16	2077.0	71.		21.3	2.66	3.7	48.6	same
17	2078.0	64.		21.1	2.67	2.6	52.2	same
18	2079.0	12.		19.2	2.70	3.2	47.8	ssivf-wgr
19	2080.0	0.05		12.7	2.67	1.0	81.7	sitstfsdy
20	2081.0	0.80		11.2	2.69	1.1	89.9	same
21	3051.0	2.26		17.2	2.67			ssivf-fgr
22	3052.0	0.53		2.3	3.17			same/sid
23	3053.0	0.19		13.0	2.68			ssivf-fgr
24	3054.0	0.87		14.9	2.66			same
25	3055.0	3.67		17.5	2.66			same
26	3056.0	0.69		14.1	2.67			same
27	3057.0	4.19		16.4	2.68			same
28	3058.0	13.		18.9	2.66			same

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CURE LABORATORIES, INC.
Petroleum Reservoir Engineering
 DALLAS, TEXAS

PAGE 2

U.S. GEOLOGICAL SURVEY
 HUSKY OIL CO., NFR OPERATOR

DATE : 14-JAN-80
 FORMATION :

FILE NO : BP-3-563
 ANALYSTS : MSP, YLS

COKE ANALYSIS RESULTS

SAMPLE NUMBER	DEPTH FEET	PERMEABILITY (MD)		POR %	GRAIN DEN.	FLUID SATS.		DESCRIPTION
		MAXIMUM	90 DEG VERTICAL			OIL	WTR	
29	3059.0	6.69		17.8	2.67			same
30	3060.0	20.		19.5	2.66			same
31	3061.0	8.66		17.1	2.67			same
32	3062.0	25.		19.8	2.66			same
33	3063.0	8.94		18.3	2.65			same
34	3064.0	1.42		14.8	2.67			same
35	3065.0	0.40		11.9	2.72			same
36	3066.0	4.95		17.2	2.65			same
37	3067.0	6.53		16.4	2.89			same;sid
38	3068.0	13.		18.3	2.69			ss;vf-fgr
39	3069.0	20.		19.1	2.65			same
40	3070.0	0.63		15.8	2.67			same
41	3071.0	0.60		16.0	2.66			same
42	3072.0	0.57		15.6	2.67			same
43	3073.0	0.33		14.0	2.69			same
44	3074.0	0.28		14.0	2.67			same
45	3075.0	0.07		9.2	2.68			ss;vf-fgr slty
46	3076.0	8.09		19.6	2.66			same
47	3077.0	1.41		16.6	2.67			same
48	3078.0	1.53		16.0	2.74			same
49	3079.0	1.19		17.1	2.66			same
50	3080.0	0.75		17.0	2.67			same
51	3081.0	1.11		17.4	2.67			same
52	3082.0	0.33		14.7	2.67			same
53	3083.0	0.07		12.4	2.77			same
54	3084.0	0.17		12.9	2.67			same
55	3085.0	0.14		13.5	2.68			same
56	3086.0	0.19		13.5	2.68			same
57	3087.0	<0.01		4.8	3.12			same;sid
58	3088.0	0.09		11.5	2.67			ss;vf-fgr slty

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COKE LABORATORIES, INC.
Petroleum Reservoir Engineering
 DALLAS, TEXAS

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FILE NO : BF-3-563
 ANALYSTS : WSP, TLS

DATE : 14-JAN-80

U.S. GEOLOGICAL SURVEY
 HUSKY OIL CO., NFR OPERATOR

COKE ANALYSIS RESULTS

SAMPLE NUMBER	DEPTH FEET	PERMEABILITY (MD)		FOR %	GRAIN DEN.	FLUID SATS.		DESCRIPTION
		MAXIMUM	90 DEG VERTICAL			OIL	WTR	
59	3089.0	0.28		15.5	2.68			same
60	3090.0	0.31		15.7	2.67			same
61	3091.0	0.16		13.5	2.68			same
62	3092.0	0.24		15.2	2.69			same
63	3093.0	0.09		11.5	2.67			same
64	3094.0	0.07		10.5	2.67			same
65	3095.0	0.14		11.5	2.67			same
66	3096.0	0.09		11.9	2.67			same

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HALLIBURTON DST REPORT

FLUID SAMPLE DATA				Date	1-9-80		Ticker Number	642692	
Sampler Pressure _____ P.S.I.G. at Surface	Kind of Job	OPEN HOLE PACKER DST		Halliburton District	ANCHORAGE				
Recovery: Cu. Ft. Gas _____	Tester	L.D. PHILLIPS		Witness	D. REED				
cc. Oil _____	Drilling Contractor	BRINKERHOFF			DR				
cc. Water _____	EQUIPMENT & HOLE DATA								
cc. Mud _____	Formation Tested	Kugrua-South Simson							
Tot. Liquid cc. _____	Elevation	50'		Ft.					
Gravity _____ * API @ _____ *F.	Net Productive Interval	15'		Ft.					
Gas/Oil Ratio _____ cu. ft./bbl.	All Depths Measured From	Kelly Bushing							
RESISTIVITY _____ CHLORIDE CONTENT _____	Total Depth	2120'		Ft.					
Recovery Water @ _____ *F. 3800 ppm	Main Hole/Casing Size	8 1/2"							
Recovery Mud @ _____ *F. 900 ppm	Drill Collar Length	433.90'		I.D. 2.25"					
Recovery Mud Filtrate @ _____ *F. _____ ppm	Drill Pipe Length	1596'		I.D. 2.602"					
Mud Pit Sample @ _____ *F. 800 ppm	Packer Depth(s)	2057-2063'		Ft.					
Mud Pit Sample Filtrate @ _____ *F. 800 ppm	Depth Tester Valve	2034'		Ft.					
Mud Weight 10.5 vis 41 SEC. ^{CP}	Surface Choke	1/8-1/4"		Bottom Choke		3/4"			
Cushion TYPE 500' AMOUNT Water	Depth Back Pres. Valve								
Recovered 306 Feet of water	Recovered 153 Feet of cut drilling mud-gas and water cut								
Recovered _____ Feet of _____	Recovered _____ Feet of _____								
Recovered _____ Feet of _____	Recovered _____ Feet of _____								
Remarks	SEE PRODUCTION TEST DATA SHEET								

Log# Section 9-20N-19W
 Lease Name MALAKPA
 Well No. 1
 Test No. 1
 Field Area MILD CAT
 County NORTH SLOPE
 State ALASKA
 Lease Owner/Company Name HUSKY OIL NPR 4 OPERATIONS
 Tested Interval 2063-2120'

TEMPERATURE	Gauge No. 2781	Gauge No. 2137		Gauge No. 7581		TIME		
	Depth: 2039 Ft.	Depth: 2043 Ft.		Depth: 2111 Ft.				
Est. *F.	24 Hour Clock		24 Hour Clock		24 Hour Clock		Tool A.M.	
	Blanked Off No		Blanked Off No		Blanked Off No		Opened 21:53 P.M.	
2116' Actual 68 *F.							Opened A.M.	
	Pressures		Pressures		Pressures		Bypass 07:48 P.M.	
	Field	Office	Field	Office	Field	Office	Reported	
Initial Hydrostatic	1131	1127.9	1133	1131.9	1141	1164.9	Minutes	
First Period Flow	Initial	237	255.2	238	259.2	276	298.7	
	Final	789	804.4	791	805.7	811	826.1	23 30
Closed in	1025	1017.1	1029	1018.4	1039	1036.8	67 61	
Second Period Flow	Initial	736	828.0	739	757.2	760	855.3	
	Final	920	927.8	923	927.8	938	945.4	207 208
Closed in	999	1018.4	1001	1018.4	1014	1035.5	298 296	
Third Period Flow	Initial							
	Final							
Closed in								
Final Hydrostatic	1183	1168.8	1186	1170.1	1217	1205.5		

FORMATION TEST DATA

FORM 161 (REV. 11-68) PRINTED IN U.S.A.

LITTLE'S PART 108 2/78

HALLIBURTON DST REPORT

FLUID SAMPLE DATA				Date	1-9-80	Ticket Number	642692
Sampler Pressure _____ P.S.I.G. at Surface				Kind of Job	OPEN HOLE	Halliburton District	ANCHORAGE
Recovery: Cu. Ft. Gas _____				Tester	L.D. PHILLIPS	Witness	D. REED
cc. Oil _____				Drilling Contractor			
cc. Water _____				BRINKERHOFF DR			
cc. Mud _____				EQUIPMENT & HOLE DATA			
Tot. Liquid cc. _____				Formation Tested	_____		
Gravity _____ ° API @ _____ °F.	Gas/Oil Ratio _____ cc. ft./bbl.			Elevation _____	Ft.		
RESISTIVITY				Net Productive Interval _____	Ft.		
CHLORIDE CONTENT				All Depths Measured From _____	Ft.		
Recovery Water _____ @ _____ °F. _____ ppm	Recovery Mud _____ @ _____ °F. _____ ppm			Total Depth _____	Ft.		
Recovery Mud Filtrate _____ @ _____ °F. _____ ppm	Mud Pit Sample _____ @ _____ °F. _____ ppm			Main Hole/Casing Size _____	Ft.		
Mud Pit Sample Filtrate _____ @ _____ °F. _____ ppm	Mud Weight _____ vis _____ cp			Drill Collar Length _____	I.D.		
				Drill Pipe Length _____	I.D.		
				Packer Depth(s) _____	Ft.		
				Depth Tester Valve _____	Ft.		
TYPE		AMOUNT	Depth Back	Surface	Bottom		
Cushion			Ft.	Pres. Valve	Choke	Choke	
Recovered	Feet of						
Recovered	Feet of						
Recovered	Feet of						
Recovered	Feet of						
Recovered	Feet of						
Remarks							
FOURTH							
TEMPERATURE	Gauge No.	7582	Gauge No.		Gauge No.		TIME
	Depth:	2117	ft.	Depth:		ft.	
Est.	°F.	24	Hour Clock	Blanked Off		Hour Clock	Tool
		Blanked Off	Yes	Blanked Off		Blanked Off	Opened
Actual	°F.	Pressures		Pressures		Pressures	
		Field	Office	Field	Office	Field	Office
Initial Hydrostatic		1144	1169.6				
First Period	Flow	Initial	281	304.3			
		Final	814	833.3			
		Closed in	1042	1040.8			
Second Period	Flow	Initial	764	862.3			
		Final	941	953.2			
		Closed in	1017	1042.0			
Third Period	Flow	Initial					
		Final					
		Closed in					
Final Hydrostatic		1221	1211.7				

Lease Name: MALAKPA
 Well No.: 1
 Field: MILDGAT
 County: NORTH SLOPE
 State: ALASKA
 Tested Interval: 2063-2120'
 Lease Owner/Company Name: HUSKY OIL NFR 4 OPERATIONS

FORM 101-REPRODUCED IN U.S.A.

FORMATION TEST DATA

LITTLE'S BOOK 100 5/79

HALLIBURTON DST REPORT

Casing perf. _____ Bottom choke 3/4" Surf. temp. -30 °F Ticket No. 642692
 Gas gravity _____ Oil gravity _____ GOR _____
 Spec. gravity _____ Chlorides _____ ppm Res. _____ @ _____ °F
 INDICATE TYPE AND SIZE OF GAS MEASURING DEVICE USED _____

Date Time	a.m. p.m.	Choke Size	Surface Pressure psi	Gas Rate MCF	Liquid Rate BPD	Remarks
21:53						Opened tool with a fair blow
22:00		1/8	400			
22:06		1/8	700			
22:07		1/4	600			
22:08		"	600			Fluid and gas to surface
22:16		"	565			Closed tool
23:23		"	600			Opened tool
23:28		"	520			
23:38		"	740			
23:51		3/8"				
23:53		"	700			Closed at surface to thaw flow line
1-10-80 00:49		"	780			Opened surface valve
00:52		1/4"	400			
01:00		"	650			Closed at surface to thaw flow line
01:05		"				Opened surface valve
01:06		"	730			Pressure-fluctuating from 670
02:48		"	750			to 750 PSI
02:50		"	720			Closed tool
06:58						Dropped shear bar and reversed out fluid
07:48						Pulled packer loose and reverse again
09:00						Broke surface equipment off, pulled up into casing and circulate
13:30						Out of hole

HALLIBURTON DST REPORT

Gauge No. 7581		Depth 2111'		Clock No. 13743		Ticket No. 642692	
First Flow Period		Second Flow Period		Third Flow Period		Third Closed In Pressure	
Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.
0 .000	298.7	0.000	355.3	0.000	366.7		
1 .0165	429.1	.0044	341.385	.0033	2.206	1017.7	
2 .0330	851.5	.0066	1030.4	.0067	1.738	1024.1	
3 .0495	851.5	.0099	1038.0	.0099	1.613	1025.3	
4 .0660	833.7	.0132	1030.4	.0133	1.517	1025.3	
5 .0825	824.8	.0166	866.785	.0167	1.441	1026.6	
6 .0990	826.1	.0199	1040.65	.0200	1.377	1026.6	
7		.0232	1031.7	.0233	1.321	1027.9	
8		.0265	1031.7	.0267	1.273	1027.9	
9		.0298	1032.9	.0300	1.230	1029.1	
10		.0331	1032.9	.0333	.529	1034.2	
11		.0364	1032.9	.2232	.359	1034.2	
12		.0695	1035.5	.4130	.275	1035.5	
13		1.026	1036.8	.6029	.223	1035.5	
14		1.358	1036.8	.7928	.187	1035.5	
15		1.689	1036.8	.9860			
		.2020	1036.8				
		.173	1036.8				

Gauge No. 7582		Depth 2117'		Clock No. 7031		Ticket No. 24	
First Flow Period		Second Flow Period		Third Flow Period		Third Closed In Pressure	
Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.
0 .000	304.3	0.000	862.3	0.000	953.2		
1 .0165	391.3	.0033	874.285	.0034	2.206	1025.5	
2 .0330	852.2	.0067	1196**	.0067	1.909	1028.0	
3 .0495	858.5	.0100	1044.6	.0101	1.733	1030.6	
4 .0660	839.6	.0134	1044.65	.0134	1.613	1031.8	
5 .0825	832.0	.0167	848.485	.0168	1.517	1033.1	
6 .0990	833.3	.0201	1047.185	.0201	1.442	1034.4	
7		.0234	1075.3	.0235	1.377	1035.7	
8		.0268	1039.5	.0268	1.322	1036.9	
9		.0301	1040.8	.0302	1.273	1038.2	
10		.0334	1040.8	.0335	1.230	1039.5	
11		.0368	1040.8	.2247	.530	1040.8	
12		.0702	1040.8	.4159	.360	1040.8	
13		1.037	1040.8	.6072	.275	1040.8	
14		1.371	1040.8	.7904	.223	1040.8	
15		1.705	1040.8	.9930	.107	1042.0	
		.2040	1040.8				
		.172	1040.8				

Reading Interval 5 * -First 11 intervals equal to 1 minute each; last 5 intervals equal to 10 minutes each.
 REMARKS: BS-Beginning of surface closure ES-End of surface closure **-.33 minutes ***-First 10 intervals equal to 1 minute each; next 4 intervals equal to 57 minutes each; last interval equal to 50 minutes.

SPECIAL PRESSURE DATA

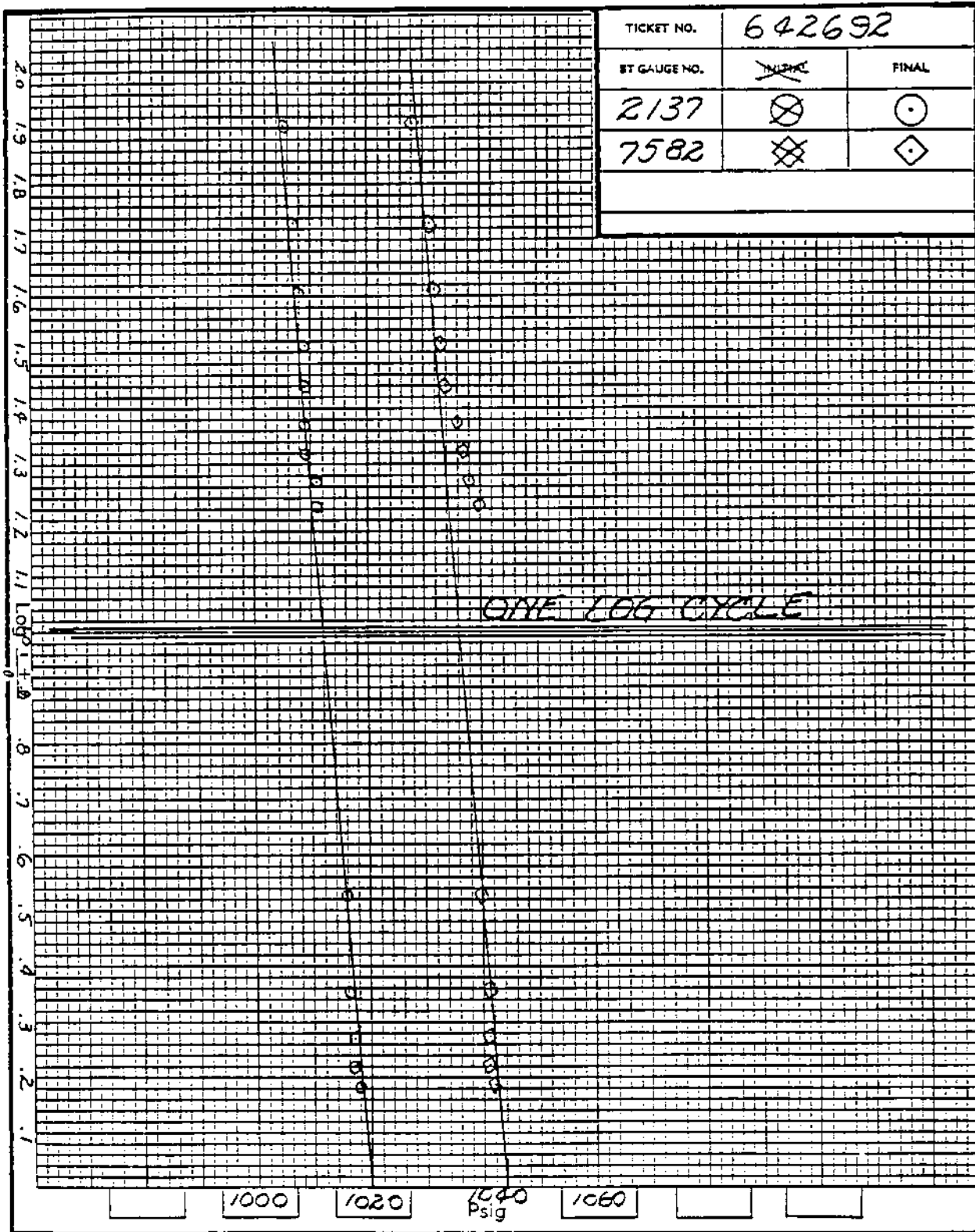
HALLIBURTON DST REPORT

Gauge No.	2781			2039'			16033			24			642692					
	First Flow Period Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	Log $1 + \frac{\beta}{\rho}$	PSIG Temp. Corr.	Time Defl. .000"	Log $1 + \frac{\beta}{\rho}$	PSIG Temp. Corr.	Time Defl. .000"	Log $1 + \frac{\beta}{\rho}$	PSIG Temp. Corr.	Time Defl. .000"	Log $1 + \frac{\beta}{\rho}$	PSIG Temp. Corr.	Time Defl. .000"	Log $1 + \frac{\beta}{\rho}$	PSIG Temp. Corr.	
0	.000	255.2	.000	804.4	.000	328.0	---	927.8	.000	---	927.8	.000	---	.000	---	927.8	.000	---
1	.016	398.6	.0033	1.485	1005.2	.044	320.205	2.206	1001.3	.0033	2.206	1001.3	.0033	.0033	2.206	1001.3	.0033	.0033
2	.032	838.5	.0065	1.198	1007.9	.107**	1010.5	1.905	1003.9	.0066	1.905	1003.9	.0066	.0066	1.905	1003.9	.0066	.0066
3	.048	828.0	.0098	1.033	1010.5	.220	1019.7	1.336	1005.2	.0098	1.336	1005.2	.0098	.0098	1.336	1005.2	.0098	.0098
4	.064	812.3	.0130	.923	1010.5	.319	1019.75	1.013	1006.5	.0131	1.013	1006.5	.0131	.0131	1.013	1006.5	.0131	.0131
5	.090	804.4	.0163	.838	1011.8	.333	999.005	1.518	1007.9	.0164	1.518	1007.9	.0164	.0164	1.518	1007.9	.0164	.0164
6	.096	804.4	.0195	.773	1011.8	.336	999.005	1.441	1007.9	.0197	1.441	1007.9	.0197	.0197	1.441	1007.9	.0197	.0197
7			.0228	.717	1011.8	.336	960.6	1.376	1007.9	.0230	1.376	1007.9	.0230	.0230	1.376	1007.9	.0230	.0230
8			.0260	.671	1011.8	.336	931.7	1.322	1009.2	.0262	1.322	1009.2	.0262	.0262	1.322	1009.2	.0262	.0262
9			.0293	.631	1013.1	.336	912.0	1.273	1010.5	.0295	1.273	1010.5	.0295	.0295	1.273	1010.5	.0295	.0295
10			.0325	.597	1013.1	.336	897.8	1.230	1010.5	.0328	1.230	1010.5	.0328	.0328	1.230	1010.5	.0328	.0328
11			.0358	.566	1013.1	.336		.529	1014.5	.0359	.529	1014.5	.0359	.0359	.529	1014.5	.0359	.0359
12			.0682	.382	1015.8	.336		.359	1015.8	.0682	.359	1015.8	.0682	.0682	.359	1015.8	.0682	.0682
13			.1007	.291	1017.1	.336		.375	1015.8	.1007	.375	1015.8	.1007	.1007	.375	1015.8	.1007	.1007
14			.1331	.236	1017.1	.336		.223	1017.1	.1331	.223	1017.1	.1331	.1331	.223	1017.1	.1331	.1331
15			.1656	.199	1017.1	.336		.187	1018.4	.1656	.187	1018.4	.1656	.1656	.187	1018.4	.1656	.1656
			.1983	.172	1017.1	.336				.1983	.172	1017.1	.1983	.1983			.1983	.1983
Gauge No.	2137		2043'	Depth	1017.1			Clock No.	13836			hour	24					
0	.000	259.2	.000	805.7	.000	757.2	---	927.8	.000	---	927.8	.000	---	.000	---	927.8	.000	---
1	.016	380.9	.0033	1.475	1003.9	.046	821.505	2.202	1001.3	.0033	2.202	1001.3	.0033	.0033	2.202	1001.3	.0033	.0033
2	.032	807.0	.0067	1.186	1007.9	.1096**	1009.2	1.903	1005.2	.0067	1.903	1005.2	.0067	.0067	1.903	1005.2	.0067	.0067
3	.048	830.6	.0099	1.029	1010.5	.2255	1019.7	1.732	1006.5	.0099	1.732	1006.5	.0099	.0099	1.732	1006.5	.0099	.0099
4	.064	813.6	.0133	.915	1011.8	.287	1019.78	1.607	1007.9	.0134	1.607	1007.9	.0134	.0134	1.607	1007.9	.0134	.0134
5	.080	805.7	.0166	.831	1013.1	.324	849.089	1.514	1009.2	.0167	1.514	1009.2	.0167	.0167	1.514	1009.2	.0167	.0167
6	.096	805.7	.0199	.765	1013.1	.341	1023.715	1.439	1009.2	.0200	1.439	1009.2	.0200	.0200	1.439	1009.2	.0200	.0200
7			.0233	.709	1013.1	.341	985.5	1.373	1009.2	.0234	1.373	1009.2	.0234	.0234	1.373	1009.2	.0234	.0234
8			.0266	.664	1014.5	.341	927.8	1.318	1009.2	.0267	1.318	1009.2	.0267	.0267	1.318	1009.2	.0267	.0267
9			.0299	.624	1014.5	.341	913.3	1.269	1010.5	.0301	1.269	1010.5	.0301	.0301	1.269	1010.5	.0301	.0301
10			.0333	.589	1014.5	.341	927.8	1.226	1010.5	.0334	1.226	1010.5	.0334	.0334	1.226	1010.5	.0334	.0334
11			.0366	.559	1014.5	.341		.527	1015.8	.0366	.527	1015.8	.0366	.0366	.527	1015.8	.0366	.0366
12			.0699	.375	1017.1	.341		.357	1015.8	.0699	.357	1015.8	.0699	.0699	.357	1015.8	.0699	.0699
13			.1032	.286	1018.4	.341		.273	1017.1	.1032	.273	1017.1	.1032	.1032	.273	1017.1	.1032	.1032
14			.1364	.231	1018.4	.341		.221	1017.1	.1364	.221	1017.1	.1364	.1364	.221	1017.1	.1364	.1364
15			.1697	.195	1018.4	.341		.186	1018.4	.1697	.186	1018.4	.1697	.1697	.186	1018.4	.1697	.1697
			.2030	.168	1018.4	.341		***		.2030	***		.2030	***			.2030	***
Reading Interval	5		2030		1018.4		35											Minutes

SPECIAL PRESSURE DATA

REMARKS: PS - Beginning of surface closure ES - End of surface closure * - First 11 intervals equal to 1 minute each; last 5 intervals equal to 10 minutes each. ** - First 10 intervals equal to 1 minute each; next 4 intervals equal to 5 minutes each. *** - First 10 intervals equal to 1 minute each; last interval equal to 58 minutes

HALLIBURTON DST REPORT

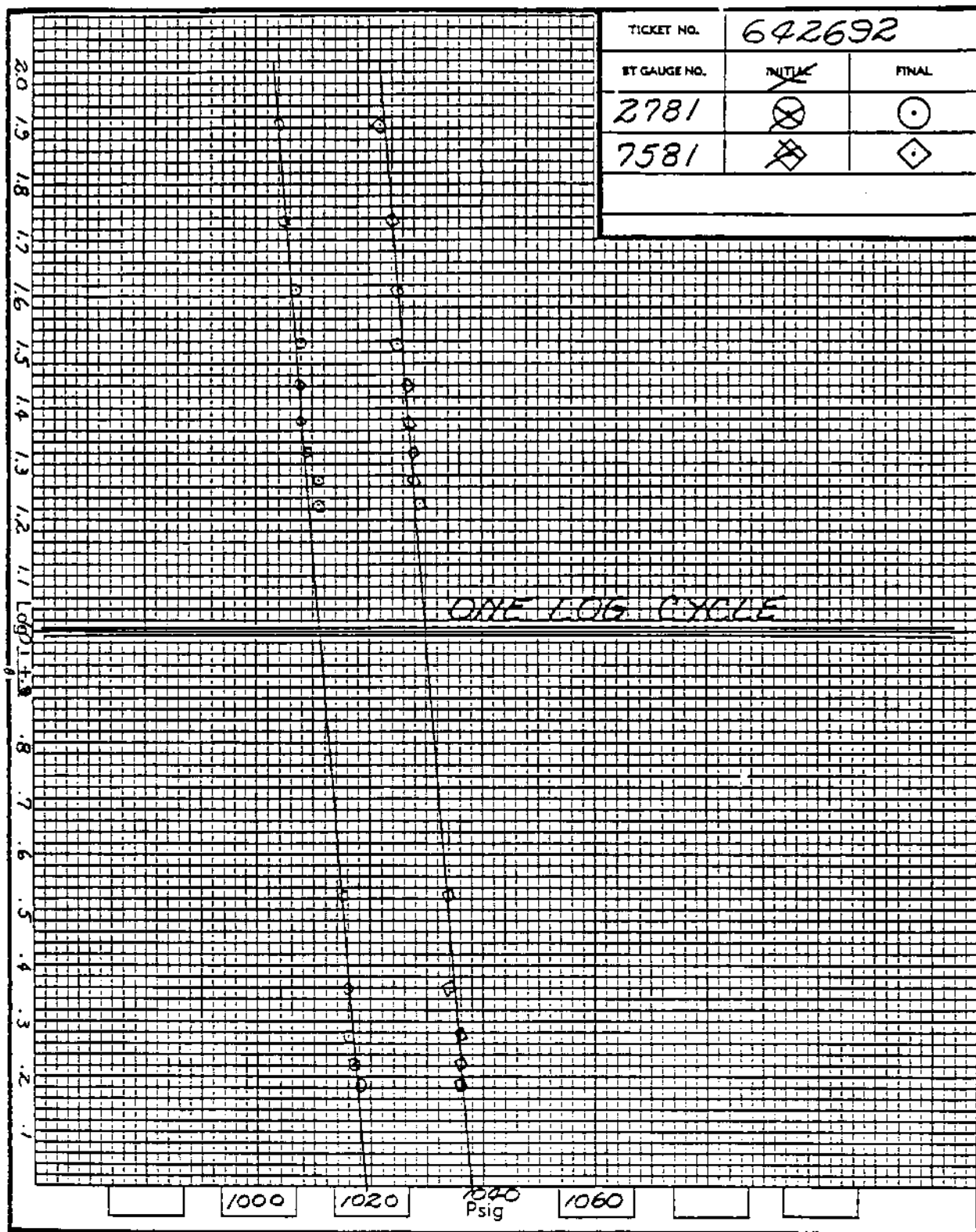


EXTRAPOLATED PRESSURE GRAPH

FORM HALLIBURTON U.S.A.

LITTLE

HALLIBURTON DST REPORT



TICKET NO.	642692	
BT GAUGE NO.	INITIAL	FINAL
2781		
7581		

EXTRAPOLATED PRESSURE GRAPH

Gas Production

HALLIBURTON DST REPORT

S.T. Gauge Numbers			2137	7582	Ticket Number		642692
Initial Hydrostatic			1132	1170	Elevation		50 ft.
Final Hydrostatic			1170	1212	Production Rate		* 1st Flow 854 MCF
1st Flow	Initial	Time	259	304	** 2nd Flow		200 MCF
	Final		806	833	3rd Flow		MCF
	Closed In Pressure		67	1018	Hole Size		8 1/2 in.
2nd Flow	Initial	Time	757	862	Footage Tested		15 ft.
	Final		207	928	Mud Weight		10.5 lb./gal.
	Closed In Pressure		298	1018	Gas Viscosity		.014 cp
3rd Flow	Initial	Time			Gas Gravity assumed		1.60
	Final				Gas Compressibility		.84
	Closed In Pressure				Temperature		168 °F
Extrapolated Static Pressure		1st					
		2nd	1020	1044			
		3rd					
Slope P/10		1st					
		2nd	1012	1036			
		3rd					

Remarks: *-First rate is based on final pressure of initial flow period.
 **-Second rate is based on observation of company personnel. First rate is questionable due to fluid being produced in gas and no separator was utilized. Calculations reported below are for each rate for the final closed in period only.

SUMMARY		B.T. Gauge No. 2137 Depth 2043'			B.T. Gauge No. 7582 Depth 2117			UNITS
PRODUCT	EQUATION	* FIRST	**SECOND	THIRD	* FIRST	**SECOND	THIRD	
Transmissibility	$\frac{Kh}{\mu} = \frac{1437 Q_g ZT}{m}$	38142.2	8932.60		37262.00	8726.47		md. ft. cp
Theoretical Flow Capacity	$Kh = \frac{Kh}{\mu} \mu$	533.91	125.06		521.67	122.17		md. ft.
Average Effective Permeability	$K = \frac{Kh}{h}$	35.60	8.34		34.778	8.15		md.
Indicated Flow Capacity	$(Kh)_i = \frac{3200 Q_g \mu ZT \log(0.472 b/r_w)}{P_i^2 - P_r^2}$	192.86	38.08		189.71	37.44		md. ft.
Damage Ratio	$DR = \frac{\text{Theo. Flow Cap}}{\text{Indicated Flow Cap (Kh)}}$	2.77	3.29		2.75	3.26		—
Indicated Flow Rate	$OF_1 = \frac{Q_g P_r^2}{P_i^2 - P_r^2}$ Max.	4957.71	1161.06		5122.00	1199.53		MCFD
	$OF_2 = \frac{Q_g P_i}{\sqrt{P_i^2 - P_r^2}}$ Min.	2057.64	481.88		2091.46	489.80		MCFD
Theoretical Potential Rate	$OF_3 = OF_1 DR$ Max.	13727.07	3813.06		14084.41	3914.11		MCFD
	$OF_4 = OF_2 DR$ Min.	5697.26	1582.57		5751.06	1598.24		MCFD
Approx. Radius of Investigation	$b \approx \sqrt{Kt}$ or $\sqrt{Kt_0}$	74.16	36.07		73.30	35.66		ft.
	$b_1 \approx \sqrt{K_1 t}$ or $\sqrt{K_1 t_0}$							ft.
Potentiometric Surface *	$Pot. = (EI - CD) + (2.319 P_s)$	372.38	372.38		354.04	354.04		ft.

NOTICE: These calculations are based upon information furnished by you and taken from Drill Stem Test pressure charts, and are furnished you for your information. In furnishing such calculations and opinions based thereon, Halliburton is merely expressing its opinion. You agree that Halliburton makes no warranty express or implied as to the accuracy of such calculations or opinions, and that Halliburton shall not be liable for any loss or damage, whether due to negligence or otherwise, in connection with such calculations and opinions.

HALLIBURTON DST REPORT

FLUID SAMPLE DATA				Date	Ticket-Number
Sampler Pressure <u>340</u> P.S.I.G. at Surface				Kind of Job	Halliburton District
Recovery: Cu. Ft. Gas _____				CASING PACKER DST	ANCHORAGE
cc. Oil _____				Tester K.C. MC WILLIAMS Witness DON MOORE	
cc. Water _____				Drilling Contractor BRINKERHOFF DRILLING COMPANY BC 5	
cc. Mud _____				EQUIPMENT & HOLE DATA TJH	
Tot. Liquid cc. _____				Formation Tested S. Simpson Sand	
Gravity _____ ° API @ _____ °F.				Elevation	<u>50'</u> KB Ft.
Gas/Oil Ratio _____ cu. ft./bbbl.				Net Productive Interval	<u>2071' - 2086'</u> Ft.
RESISTIVITY _____ CHLORIDE CONTENT _____				All Depths Measured From	<u>Kelly Bushing</u>
Recovery Water @ _____ °F. ppm				Total Depth	<u>2231'</u> PB Ft.
Recovery Mud @ _____ °F. ppm				Main Hole/Casing Size	<u>7"</u>
Recovery Mud Filtrate @ _____ °F. ppm				Drill Collar Length	<u>291'</u> I.D. <u>2.125"</u>
Mud Pit Sample @ _____ °F. ppm				Drill Pipe Length	<u>1700'</u> I.D. <u>2.764"</u>
Mud Pit Sample Filtrate @ _____ °F. <u>475</u> ppm				Packer Depth(s)	<u>2042'</u> Ft.
Mud Weight <u>10.2</u> via <u>44</u> SEC XXX				Depth Tester Valve	<u>2010'</u> Ft.
TYPE AMOUNT		Depth Back		Surface	Bottom
Cushion Water	<u>500</u>	Ft.	Pres. Valve	Choke	<u>.75"</u>
Recovered	Feet of	<div style="border: 2px solid black; padding: 10px; display: inline-block;"> <p style="font-size: 2em; margin: 0;">MAILED</p> <p style="margin: 5px 0;">FEB 15 1980</p> <p style="font-size: 0.8em; margin: 0;">HALLIBURTON SERVICES</p> <p style="font-size: 0.7em; margin: 0;">BUREAU OF OILFIELD</p> </div>			
Recovered	Feet of				
Recovered	Feet of				
Recovered	Feet of				
Recovered	Feet of				
Remarks <u>SEE PRODUCTION TEST DATA SHEET</u>					
Q = Questionable CS = Clock stopped CTE = Chart time expired					
TEMPERATURE					
Gauge No. <u>82</u>		Gauge No. <u>32</u>		Gauge No. <u>13</u>	
Depth: <u>2024</u> Ft.		Depth: <u>2028</u> Ft.		Depth: <u>2095</u> Ft.	
TIME		TIME		TIME	
144 Hour Clock		48 Hour Clock		144 Hour Clock	
Tool <u>1-31-80</u> A.M.		Tool <u>1-31-80</u> A.M.		Tool <u>1-31-80</u> A.M.	
Est. _____ °F.		Est. _____ °F.		Est. _____ °F.	
Blanked Off <u>NO</u>		Blanked Off <u>NO</u>		Blanked Off <u>YES</u>	
Actual <u>2103</u> °F.		Actual <u>2103</u> °F.		Actual <u>2103</u> °F.	
Pressures		Pressures		Pressures	
Reported		Reported		Reported	
Computed		Computed		Computed	
Initial Hydrostatic		Initial Hydrostatic		Initial Hydrostatic	
Field <u>1124.1</u>		Field <u>1086</u>		Field <u>1094</u>	
Office <u>1147.2</u>		Office <u>1093.9</u>		Office <u>1147.2</u>	
Initial Flow		Initial Flow		Initial Flow	
Field <u>255.9</u>		Field <u>238</u>		Field <u>239</u>	
Office <u>283.5</u>		Office <u>253.5</u>		Office <u>283.5</u>	
Final Flow		Final Flow		Final Flow	
Field <u>156.8</u>		Field <u>143</u>		Field <u>141</u>	
Office <u>156.3</u>		Office <u>148.1</u>		Office <u>156.3</u>	
Closed in		Closed in		Closed in	
Field <u>1026.9</u>		Field <u>1014</u>		Field <u>1024</u>	
Office <u>1026.4</u>		Office <u>1017.5</u>		Office <u>1026.4</u>	
Initial Flow		Initial Flow		Initial Flow	
Field <u>210.2</u>		Field <u>143</u>		Field <u>159</u>	
Office <u>234.1</u>		Office <u>202.0</u>		Office <u>234.1</u>	
Final Flow		Final Flow		Final Flow	
Field <u>86.0</u>		Field <u>79</u>		Field <u>88</u>	
Office <u>285</u>		Office <u>81.6</u>		Office <u>90.1</u>	
Closed in		Closed in		Closed in	
Field <u>1011.8</u>		Field <u>999</u>		Field <u>1015</u>	
Office <u>1016.7</u>		Office <u>1002.3</u>		Office <u>1016.7</u>	
Initial Flow		Initial Flow		Initial Flow	
Field <u>646.4-Q</u>		Field <u>143</u>		Field <u>141</u>	
Office <u>689.5-Q</u>		Office <u>805.0-Q</u>		Office <u>689.5-Q</u>	
Final Flow		Final Flow		Final Flow	
Field <u>334.4</u>		Field <u>-</u>		Field <u>327</u>	
Office <u>2870</u>		Office <u>407.2-CTE</u>		Office <u>340.1</u>	
Closed in		Closed in		Closed in	
Field <u>1021.5</u>		Field <u>-</u>		Field <u>1015</u>	
Office <u>2880</u>		Office <u>-</u>		Office <u>1025.5</u>	
Final Hydrostatic		Final Hydrostatic		Final Hydrostatic	
Field <u>1124.1</u>		Field <u>-</u>		Field <u>1147</u>	
Office <u>1147.2</u>		Office <u>CTE</u>		Office <u>1147.2</u>	

Legal Location Sec. 10 Twp. 10 Rng. 10
 Lease Name MALAKPA
 Well No. 1
 Test No. 2
 Tested Interval 2042' - 2231'
 County NORTH SLOPE
 State ALASKA
 Lease Owner/Company Name HUSKY OIL OPERATIONS

HALLIBURTON DST REPORT

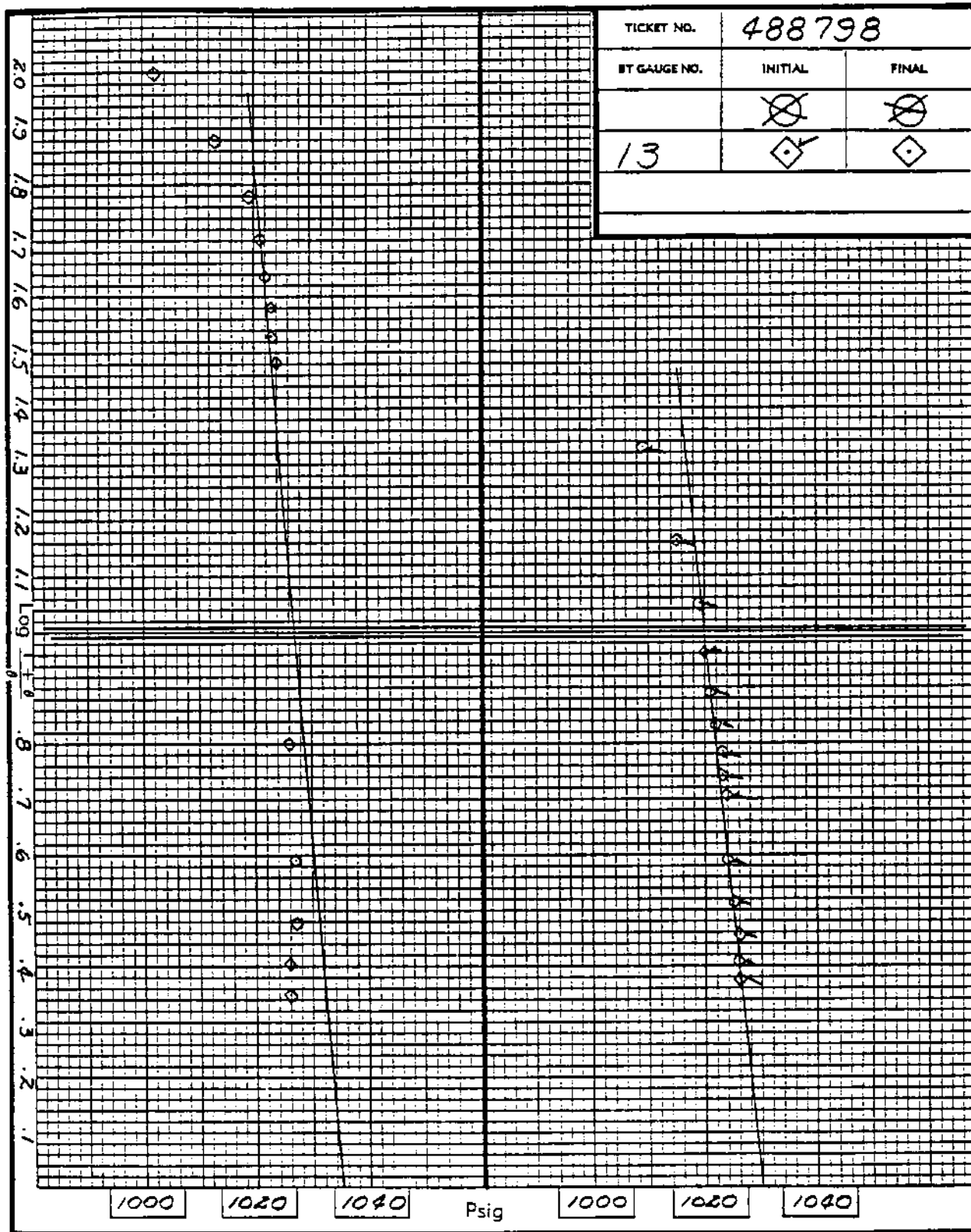
FLUID SAMPLE DATA		Date	1-31-80	Ticket Number	488798
Sampler Pressure _____ P.S.I.G. at Surface		Kind of Job	CASING PACKER DST	Halliburton District	ANCHORAGE
Recovery: Cu. Ft. Gas _____		Tester	MR. MC WILLIAMS	Witness	MR. MOORE
cc. Oil _____		Drilling Contractor	BRINKERHOFF DRILLING COMPANY BC		
cc. Water _____		EQUIPMENT & HOLE DATA			
cc. Mud _____		Formation Tested	_____		
Tot. Liquid cc. _____		Elevation	_____ Ft.		
Gravity _____ * API @ _____ *F.	Gas/Oil Ratio _____ cu. ft./bbl.	Net Productive Interval	_____ Ft.		
RESISTIVITY		All Depths Measured From	_____ Ft.		
CHLORIDE CONTENT		Total Depth	_____ Ft.		
Recovery Water _____ @ _____ *F. _____ ppm	Recovery Mud _____ @ _____ *F. _____ ppm	Main Hole/Casing Size	_____		
Recovery Mud Filtrate _____ @ _____ *F. _____ ppm	Mud Pit Sample _____ @ _____ *F. _____ ppm	Drill Collar Length _____ I.D.	_____		
Mud Pit Sample Filtrate _____ @ _____ *F. _____ ppm	Mud Weight _____ vis _____ cp	Drill Pipe Length _____ I.D.	_____		
		Packer Depth(s) _____ Ft.	_____		
		Depth Tester Valve _____ Ft.	_____		

TYPE	AMOUNT	Depth Back Ft.	Surface Pres. Valve	Surface Choke	Bottom Choke
Cushion					
Recovered	Feet of				
Recovered	Feet of				
Recovered	Feet of				
Recovered	Feet of				
Recovered	Feet of				
Remarks					
Q = Questionable CS = Clock stopped					

FOURTH GAUGE:							
TEMPERATURE	Gauge No. 74	Gauge No.	Gauge No.	TIME			
	Depth: 2099' Ft.	Depth: _____ Ft.	Depth: _____ Ft.	_____ Hour Clock	_____ Hour Clock	_____ Hour Clock	_____ A.M.
Est. _____ *F.	Blanked Off	Yes	Blanked Off	Blanked Off	Blanked Off	Blanked Off	Tool _____ A.M.
Actual _____ *F.	Pressures		Pressures		Pressures		Opened _____ P.M.
	Field	Office	Field	Office	Field	Office	Opened _____ A.M.
Initial Hydrostatic		1138.5					Bypass _____ P.M.
First Period	Flow Initial	295.3					Reported _____ Minutes
	Flow Final	156.7					Computed _____ Minutes
	Closed in	1029.8					
Second Period	Flow Initial	234.5					
	Flow Final	91.6					
	Closed in	1020.2					
Third Period	Flow Initial	789.1-0					
	Flow Final	416.8-65					
	Closed in	-					
Final Hydrostatic		1138.5					

Log Location Sec. 1 sp. 1-100
 Lease Name MALAKPA
 Well No. 1
 Test No. 2
 Tail No. 2042' - 2231' PB
 Taild Interval
 County NORTH SLOPE
 State ALASKA
 Lease Owner/Company Name HUSKY OIL NPR-4 OPERATIONS

HALLIBURTON DST REPORT



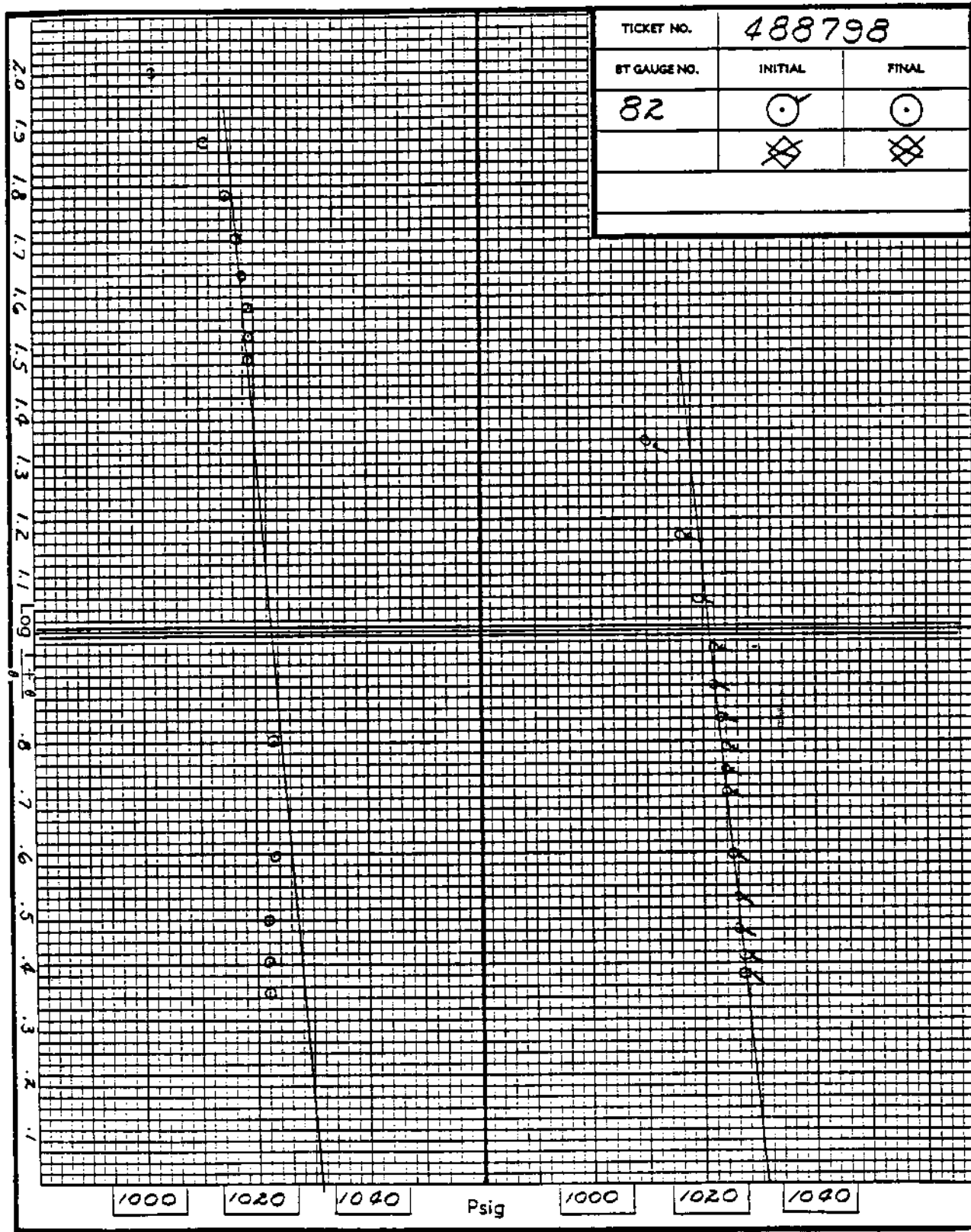
EXTRAPOLATED PRESSURE GRAPH

FORM HALLIBURTON 10-0-54

LITTLE

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HALLIBURTON DST REPORT



TICKET NO.	488798	
BT GAUGE NO.	INITIAL	FINAL
82		

EXTRAPOLATED PRESSURE GRAPH

LITTLE 5

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HALLIBURTON DST REPORT

Gauge No.	82			2024'			20040			144 hour			488798		
	Flow Period Time Defl. PSIG Temp. Corr.	Time Defl. 000"	Log $\frac{1+\beta}{\beta}$	Time Defl. 000"	PSIG Temp. Corr.	Time Defl. 000"	Log $\frac{1+\beta}{\beta}$	Time Defl. 000"	PSIG Temp. Corr.	Time Defl. 000"	PSIG Temp. Corr.	Time Defl. 000"	Log $\frac{1+\beta}{\beta}$	Time Defl. 000"	PSIG Temp. Corr.
0	.0000	255.9	1.56.8	.0000	210.2	.0000	86.0	.0000	646.4-0	.0000	334.4	.0000	.0000	334.4	
1	(.0060	260.3	945.7	(.0130	157.9)C	.0061	1.812***	.0061	(.0380	201.5)C	.0067	2.476	.0067	906.7	
2	.0337	980.4*	1009.7	.0226	159.0	.0229	1.256	.0229	(.0560	312.6)C	.0134	2.176	.0134	986.9	
3	(.0360	983.7	1016.1	(.0270	161.2)C	.0397	1.034	.0397	(.0650	394.3)C	.0201	2.002	.0201	1002.1	
4	.0617	169.9	1019.4	.0452	162.3	.0564	.898	.0564	(.0780	513.0)C	.0268	1.878	.0268	1010.7	
5	(.0640	169.9)C	1021.5	.0678	135.0	.0732	.801	.0732	.2015	396.5**	**0335	1.783	**0335	1015.1	
6	.0898	110.0	1021.5	.0905	106.7	.0899	.727	.0899	.4024	413.9	.0402	1.705	.0402	1017.2	
7	(.0960	107.8)C	1022.6	(.1030	100.2)C	.1067	.668	.1067	.6034	415.0	.0469	1.640	.0469	1018.3	
8	(.1090	503.2)C	1023.7	.1131	96.9	.1235	.619	.1235	.8043	412.8	.0536	1.583	.0536	1019.4	
9	.1178	185.1	1023.7	.1357	91.5	.1402	.578	.1402	1.0052	403.0	.0603	1.533	.0603	1019.4	
10	.1459	202.6	1023.7	.1600	86.0***	.1570	.542	.1570	(1.1140	401.9)C	.0670	1.489	.0670	1019.4	
11	.1739	196.0	1024.8	.1737	81.6	.1737	.511	.1737	1.2052	366.0	.3742	.802	.3742	1022.6	
12	.2020	166.6	1025.9	.1905	89.8	.1905	.484	.1905	1.4071	368.1	.6814	.595	.6814	1022.6	
13	(.2120	167.7)C	1025.9	.2072	86.0	.2072	.460	.2072	(1.4740	361.6)C	.9885	.480	.9885	1021.5	
14	.2300	156.8	1026.9	.2240	81.6	.2240	.438	.2240	1.6080	334.4	1.2957	.405	1.2957	1021.5	
15			1026.9												

Gauge No.	32			2028			48 hour			
	Flow Period Time Defl. PSIG Temp. Corr.	Time Defl. 000"	Log $\frac{1+\beta}{\beta}$	Time Defl. 000"	PSIG Temp. Corr.	Time Defl. 000"	Log $\frac{1+\beta}{\beta}$	Time Defl. 000"	PSIG Temp. Corr.	
0	.0000	253.5	148.1	.0000	202.0	.0000	81.6	.0000	805.0-0	
1	(.0130	251.1)C	979.4	(.0380	148.9)C	.0185	1.807***	.0185	(.1130	198.1)C
2	.1013	974.6*	1003.9	.0671	152.1	.0691	1.253	.0691	(.1640	308.2)C
3	(.1030	975.4)C	1008.7	(.0780	154.5)C	.1197	1.031	.1197	(.1910	390.6)C
4	.1857	161.6	1010.3	.1343	154.5	.1703	.895	.1703	(.2290	507.1)C
5	(.1930	160.8)C	1011.1	.2014	126.7	.2200	.798	.2200	.6053	388.2**
6	.2700	100.6	1011.9	.2685	99.8	.2714	.724	.2714	1.2090	406.5
7	(.2870	99.0)C	1012.7	(.2980	94.2)C	.3220	.665	.3220	1.8127	408.0
8	(.3250	496.8)C	1013.5	.3357	90.3	.3726	.616	.3726	1.9930	407.2)
9	.3544	178.2	1013.5	.4028	86.3	.4231	.575	.4231		
10	.4388	194.1	1013.5	.4750	81.6**	.4737	.540	.4737		
11	.5232	188.5-0	1015.1	.5243	81.6	.5243	.509	.5243		
12	.6076	158.4	1015.9	.5740	81.6	.5740	.482	.5740		
13	(.6340	158.4)C	1015.9	.6254	81.6	.6254	.457	.6254		
14	.6920	148.1	1016.7	.6760	81.6	.6760	.436	.6760		
15			1017.5							

Gauge No.	50
Reading Interval	50
Minutes	359

REMARKS: Int. = 60 min. **First 10 int. = 10 min. each; next 4 int. = 40 min. each; last int. = 37 min. ***Int. = 43 min.
 ****Int. = 11 min. *****first 10 int. = 12 min. each; next 4 int. = 550 min. each; last int. = 559 minutes.

SPECIAL PRESSURE DATA

UNITED STATES PATENT OFFICE

HALLIBURTON DST REPORT

Cauge No.	13		Depth		2095'		Clock No.		20039		144 hour		Ticket No.		488798	
	Flow Period		Closed In Pressure		Second Flow Period		Closed In Pressure		Third Flow Period		Third Flow Period		Closed In Pressure		PSIG Temp. Corr.	
	Time Defl. .000"	PSIG Temp. Corr.	Log t + θ	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Log t + θ	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Time Defl. .000"	PSIG Temp. Corr.	Log t + θ	PSIG Temp. Corr.
0	.0000	283.5	---	156.3	.0000	234.1	---	90.1	.0000	689.5-0	---	340.1	.0000	---	---	340.1
1	(.0040	284.4(L)	1.624	957.6	(.0130	170.4(C)	1.804***	477.0	.0062	207.5(C)	---	2.477	.0067	2.477	---	861.5
2	.0337	998.2*	1.333	1008.8	.0225	170.4	1.253	813.0	.0230	319.7(C)	---	2.174	.0135	2.174	---	986.7
3	(.0360	1000.8)	1.165	1014.9	(.0270	172.2(C)	1.032	910.0	.0398	401.9(C)	---	2.000	.0202	2.000	---	1001.7
4	.0617	179.3	1.050	1018.5	.0449	172.2	.895	955.8	.0567	518.5(C)	---	1.878	.0269	1.878	---	1013.2
5	(.0650	172.2(C)	.963	1020.2	.0674	136.9	.799	979.6	.0735	401.0***	---	1.781	**.0337	1.781	---	1019.3
6	.0898	112.1	.893	1021.1	.0899	107.7	.725	992.9	.0903	418.7	---	1.704	.0404	1.704	---	1021.1
7	(.0960	109.5(C)	.835	1022.0	(.1010	101.5(C)	.665	999.0	.1072	421.3	---	1.639	.0471	1.639	---	1022.0
8	(.1090	506.1(C)	.786	1022.9	.1124	97.1	.617	1005.2	.1240	418.7	---	1.581	.0539	1.581	---	1022.9
9	.1178	189.9	.744	1022.9	.1348	91.8	.576	1009.6	.1408	410.7	---	1.532	.0605	1.532	---	1022.9
10	.1459	204.0	.707	1023.8	.1590	90.1***	.540	1012.3	.1577	410.7(C)	---	1.487	.0674	1.487	---	1023.8
11	.1739	198.7-C	.678	1023.8	.1745	88.7	.509	1014.1	.1745	372.7	---	1.401	.0761	1.401	---	1026.4
12	.2020	166.9	.612	1024.6	.1913	82.7	.482	1014.9	.1913	372.7	---	1.359	.0848	1.359	---	1027.3
13	(.2100	167.8(P)	.556	1025.5	.2082	81.8	.458	1015.8	.2082	368.3(C)	---	1.302	.0935	1.302	---	1027.3
14	.2300	156.3	.462	1026.4	.2250	78.7	.436	1016.7	.2250	340.1	---	1.250	1.3022	1.250	---	1026.4
15			.376	1026.4							---	1.160	1.6160	1.160	---	1025.5
Cauge No.	74	Depth	2099'	40	Clock No.	9397	48 hour									
0	.0000	295.3	---	156.7	.0000	234.5	---	91.6	.0000	789.1-0	---	---	.0000	---	---	---
1	(.0110	283.5	1.630	994.6	(.0420	168.4(C)	1.816***	523.3	.0186	216.4(C)	---	---	(.1130	---	---	---
2	.1017	1005.3	1.339	1017.0	.0678	174.8	1.255	824.1	.0692	327.2(C)	---	---	(.1650	---	---	---
3	(.1050	1006.3	1.172	1021.3	(.0820	176.9(C)	1.199	919.4	.1199	410.4(C)	---	---	(.1920	---	---	---
4	.1865	172.7	1.057	1022.3	.1357	174.8	.897	963.9	.1705	526.6(C)	---	---	(.2280	---	---	---
5	(.1950	173.7)	.9835	1023.4	.2035	136.4	.800	986.2	.2212	406.1***	---	---	.6077	---	---	---
6	.2712	109.8	.900	1024.5	.2714	108.7	.726	997.8	.2718	416.8)	---	---	(.0160	---	---	---
7	(.2900	108.7)	.842	1024.5	(.2990	102.3(C)	.667	1004.2	.3225	---	---	---	---	---	---	---
8	.3260	511.6)	.793	1025.5	.3392	99.1	.618	1010.6	.3731	---	---	---	---	---	---	---
9	.3560	192.9	.750	1025.5	.4071	94.8	.577	1014.9	.4238	---	---	---	---	---	---	---
10	.4407	206.8	.713	1025.5	.4800	91.6***	.541	1015.9	.4744	---	---	---	---	---	---	---
11	.5255	200.4-	.599	1026.6	.5251	88.7	.510	1017.0	.5251	---	---	---	---	---	---	---
12	.6102	168.4	.520	1027.7	.5757	83.3	.483	1018.1	.5757	---	---	---	---	---	---	---
13	(.6360	169.5)	.461	1027.7	.6264	78.7	.459	1019.1	.6264	---	---	---	---	---	---	---
14	.6950	156.7	.415	1028.7	.6770	74.7	.437	1020.2	.6770	---	---	---	---	---	---	---
15			.380	1029.8							---	---				
Reading Interval	50			40			30									Minutes

REMARKS: *Int. = 60 min. **First 10 int. = 10 min. each; next 4 int. = 40 min. each; last int. = 37 min. ***Int. = 43 min.
 ****Int. = 11 min. *****Int. = 360 min. ****First 10 int. = 12 min. each; next 4 int. = 550 min. each; last int. = 559 minutes.

SPECIAL PRESSURE DATA

FORM 103 RE PRINTED 10-6-64

Gas Production

HALLIBURTON DST REPORT

B.T. Gauge Numbers			82	13	Ticket Number		488798
Initial Hydrostatic			1124.1	1147.2	Elevation		50 ft.
Final Hydrostatic			1124.1	1147.2	Production Rate		1st Flow 335 MCF
1st Flow	Initial	Time	255.9	283.5	2nd Flow		- MCF
	Final	410	156.8	156.3	3rd Flow		330 MCF
	Closed In Pressure	297	1026.9	1026.4	Hole Size		7 in.
2nd Flow	Initial	Time	210.2	234.1	Footage Tested		15 ft.
	Final	283	86.0	90.1	Mud Weight		10.2 lbs./gal.
	Closed In Pressure	401	1011.8	1016.7	Gas Viscosity		0.014 cp
3rd Flow	Initial	Time	646.4-Q	689.5-Q	Gas Gravity		0.65 Estimated
	Final	2873	334.4	340.1	Gas Compressibility		0.815
	Closed In Pressure	2879	1021.5	1025.5	Temperature		65 °F
Extrapolated Static Pressure	1st		1031	1030			
	2nd		-	-			
	3rd		1031	1035			
Slope P/10	1st		1021	1020			
	2nd		-	-			
	3rd		1023	1027			

Remarks:

Q = Questionable

SUMMARY		B.T. Gauge No. 82 Depth 2024'			B.T. Gauge No. 13 Depth 2095'			UNITS
PRODUCT	EQUATION	FIRST	SECOND	THIRD	FIRST	SECOND	THIRD	
Transmissibility	$Kh/\mu = \frac{1637 Q_g ZT}{m}$	11434.9		14066.6	11446.1		14012.0	md. ft. / cp
Theoretical Flow Capacity	$Kh = \frac{K_h}{\mu}$	160.089		196.933	160.245		196.169	md. ft.
Average Effective Permeability	$K = \frac{K_h}{h}$	-		-	-		-	md.
Indicated Flow Capacity	$(Kh)_i = \frac{3200 Q_g \mu ZT \text{Log}(0.472 b/r_w)}{P_p^2 - P_r^2}$	12.829		17.277	12.852		17.195	md. ft.
Damage Ratio	$DR = \frac{\text{Theo. Flow Cap}}{\text{Indicated Flow Cap}} \frac{Kh}{(Kh)_i}$	12.480		11.399	12.470		11.409	-
Indicated Flow Rate	$OF_1 = \frac{Q_g}{P_p^2 - P_r^2} P_p^2$ Max.	343		369	343		370	MCFD
	$OF_2 = \frac{Q_g P_p}{\sqrt{P_p^2 - P_r^2}}$ Min.	339		349	339		349	MCFD
Theoretical Potential Rate	$OF_3 = OF_1 DR$ Max.	4280		4203	4275		4220	MCFD
	$OF_4 = OF_2 DR$ Min.	4230		3976	4226		3986	MCFD
Approx. Radius of Investigation	$b \approx \sqrt{Kt}$ or $\sqrt{Kt_0}$	-		-	-		-	ft.
	$b_1 \approx \sqrt{K_1 t}$ or $\sqrt{K_1 t_0}$	66		217	66		216	ft.
Potentiometric Surface *	$Pot. = (EI - GD) + (2.319 P_s)$	417		417	344		355	ft.

NOTICE: These calculations are based upon information furnished by you and taken from Drill Stem Test pressure charts, and are furnished you for your information. In furnishing such calculations and evaluations based thereon Halliburton is merely expressing its opinion. You agree that Halliburton makes no warranty express or implied as to the accuracy of such calculations or opinions, and that Halliburton shall not be liable for any loss or damage, whether due to negligence or otherwise, in connection with such calculations and opinions.



CHEMICAL & GEOLOGICAL LABORATORIES OF ALASKA, INC.

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TELEPHONE (907)-279-4014
274-3364

ANCHORAGE INDUSTRIAL CENTER
5633 B Street

ANALYTICAL REPORT

From Husky Oil Company Product Fluid Samples
Address Anchorage, Alaska Date January 22, 1980
Other Pertinent Data _____
Analyzed by IMG Date January 29, 1980 Lab No. 2664

REPORT OF ANALYSIS
FLUID SAMPLES
DST #1 (2066-2120)
WALAKPA NO. 1
NPRA, ALASKA

SAMPLEMilligrams/liter.....	
	<u>CHLORIDE</u>	<u>OIL & GREASE (*)</u>
Top of DCIP Valve	14800	386
Reverse Out Water	7600	86
Mud	660	—
Water Cushion	210	—

(*) Diesel Fuel



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GAS ANALYSIS REPORT

Company Husky Oil Company Date February 14, 1980 Lab No. 2788-1
 Well No. Walakpa No. 1 Location _____
 Field NEPA Formation _____
 County _____ Depth DST No. 2 (2073-88)
 State Alaska Sampling Point 30 Min. Open on 3rd Flow
 Line pressure _____ psig; Sample pressure 147 psig; Temperature _____ °F; Container number _____
 Remarks Sample No. 3

Component	Mole % or Volume %	Gallons per MCF
Oxygen.....	0	
Nitrogen.....	1.27	
Carbon dioxide.....	Trace	
Hydrogen sulfide.....	—	
<u>Helium</u>	<u><0.01</u>	
Methane.....	98.72	
Ethane & Higher.....	0.01	
Total.....		
100.00		
GPM of pentanes & higher fraction.....		
Gross btu cu. ft. @ 60° F. & 14.7 psia (dry basis).....		997
Specific gravity (calculated from analysis).....		0.559
Specific gravity (measured).....		0.550

Remarks _____



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ANALYTICAL REPORT

From Husky Oil Company Product Fluid
Address Anchorage, Alaska Date February 5, 1980
Other Pertinent Data _____
Analyzed by DB/TMG Date February 13, 1980 Lab No. 2788

**REPORT OF ANALYSIS
FLUID SAMPLES
WALAKPA NO. 1
NPRA, ALASKA**

Samples received February 5, 1980
Samples taken February 1, 1980 (DST #2 2073-38 feet)

<u>SAMPLE</u>	<u>CHLORIDE, mg/l</u>
Cushion Water	300
Drilling Mud	480



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ANALYTICAL REPORT

From Husky Oil Company Product Water
Address Anchorage, Alaska Date February 8, 1980
Other Pertinent Data _____
Analyzed by IMG Date February 14, 1980 Lab No. 2844

REPORT OF ANALYSIS
WATER SAMPLES
WALAKPA NO. 1
NORTH SLOPE, ALASKA

Samples received February 8, 1980
Samples taken from DST No. 2

<u>SAMPLE</u>	<u>RESISTIVITY, ohm-cm @ 68°F</u>	<u>CHLORIDE, mg/l</u>
Sample Chamber	0.32	15400
Test Tool Sub.	0.72	6300



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5633 B Street

ANALYTICAL REPORT

WALAKPA #1

From Husky Oil Company Product Cores - for fresh water susceptibility
Address Anchorage, Alaska Date February 1980 analysis.
Other Pertinent Data _____

Analyzed by PG Date March 4, 1980 Lab No. 3047

REPORT OF ANALYSIS
CORE SAMPLES
WALAKPA NO. 1
NPRA, ALASKA

PROCEDURE:

Selected core samples were analyzed to determine the susceptibility of existing materials to the exposure of various liquids.

LEGEND:

Fresh Water = (City of Anchorage) See Attached Analysis.
CaCl₂ = Calcium Chloride (36.11% Calcium, 63.89% Chloride)
CaCl₂ 25000 = 25000 ppm as CaCl₂ = 9027.5 ppm as Ca - 15972.5 ppm as Cl
NaCl = Sodium Chloride (39.34% Sodium, 60.66% Chloride)
KCl = Potassium Chloride (52.25% Potassium, 47.75% Chloride)
Filtrate = Drilling Mud Filtrate



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ANCHORAGE INDUSTRIAL CENTER
5833 B Street

ANALYTICAL REPORT

CUSTOMER Husky Oil Company SAMPLE LOCATION: City of Anchorage

DATE COLLECTED — TIME COLLECTED: —

SAMPLED BY — SOURCE —

REMARKS Potable Water

FOR LAB USE ONLY	
RECVD. BY	LAB # <u>CITY WATER</u>
DATE RECEIVED	<u> — </u>
DATE COMPLETED	<u> — </u>
DATE REPORTED	<u> — </u>
SIGNED	<i> Archie P. Hansen </i>

mg/l	mg/l	mg/l
<input type="checkbox"/> Ag, Silver	<input type="checkbox"/> P, Phosphorous	<input type="checkbox"/> Cyanide
<input type="checkbox"/> Al, Aluminum	<input type="checkbox"/> Pb, Lead	<input checked="" type="checkbox"/> Sulfate <u> 17 </u>
<input type="checkbox"/> As, Arsenic	<input type="checkbox"/> Pt, Platinum	<input type="checkbox"/> Phenol
<input type="checkbox"/> Au, Gold	<input type="checkbox"/> Sb, Antimony	<input checked="" type="checkbox"/> Total Dissolved Solids <u> 36 </u>
<input type="checkbox"/> B, Boron	<input type="checkbox"/> Se, Selenium	<input type="checkbox"/> Total Volatile Solids
<input type="checkbox"/> Ba, Barium	<input type="checkbox"/> Si, Silicon	<input type="checkbox"/> Suspended Solids
<input type="checkbox"/> Bi, Bismuth	<input type="checkbox"/> Sn, Tin	<input type="checkbox"/> Volatile Suspended Solids
<input checked="" type="checkbox"/> Ca, Calcium <u> 28 </u>	<input type="checkbox"/> Sr, Strontium	<input checked="" type="checkbox"/> Hardness as CaCO ₃ <u> 98 </u>
<input type="checkbox"/> Cd, Cadmium	<input type="checkbox"/> Ti, Titanium	<input checked="" type="checkbox"/> Alkalinity as CaCO ₃ <u> 55 </u>
<input type="checkbox"/> Co, Cobalt	<input type="checkbox"/> W, Tungsten	<input type="checkbox"/> _____
<input type="checkbox"/> Cr, Chromium	<input type="checkbox"/> V, Vanadium	<input type="checkbox"/> _____
<input type="checkbox"/> Cu, Copper	<input type="checkbox"/> Zn, Zinc	<input type="checkbox"/> _____
<input checked="" type="checkbox"/> Fe, Iron <u> <0.1 </u>	<input type="checkbox"/> Zr, Zirconium	<input type="checkbox"/> _____
<input type="checkbox"/> Hg, Mercury	<input type="checkbox"/> Ammonia Nitrogen-N	<input checked="" type="checkbox"/> Ohms Conductivity <u> 140 </u>
<input checked="" type="checkbox"/> K, Potassium <u> 0.8 </u>	<input type="checkbox"/> Kjeldahl Nitrogen-N	<input checked="" type="checkbox"/> pH Units <u> 6.8 </u>
<input checked="" type="checkbox"/> Mg, Magnesium <u> 4.5 </u>	<input type="checkbox"/> Nitrate-N	<input type="checkbox"/> Turbidity NTU
<input type="checkbox"/> Mn, Manganese	<input type="checkbox"/> Nitrite-N	<input type="checkbox"/> Color Units
<input type="checkbox"/> Mo, Molybdenum	<input type="checkbox"/> Phosphorus (Ortho)-P	<input type="checkbox"/> T. Coliform/100ml
<input checked="" type="checkbox"/> Na, Sodium <u> 2.5 </u>	<input checked="" type="checkbox"/> Chloride <u> 2 </u>	<input type="checkbox"/> _____
<input type="checkbox"/> Ni, Nickel	<input type="checkbox"/> Fluoride	<input type="checkbox"/> _____

3 PERMEABILITY REDUCTION

LAB NO. 3047-1

<u>DEPTH = 2078 Feet</u>	<u>TIME</u>		
	<u>15 Min.</u>	<u>30 Min.</u>	<u>One Hour</u>
Fresh Water	85.2	88.3	89.2
CaCl ₂ 25000	49.0	59.3	68.8
CaCl ₂ 50000	23.6	47.0	53.3
CaCl ₂ 100000	20.9	44.6	50.6
NaCl 50000	22.2	46.6	51.5
KCl 50000	23.0	47.0	52.3
Filtrate	50.1	80.2	91.0

<u>DEPTH = 2075 Feet</u>			
Fresh Water	58.7	85.0	90.1
CaCl ₂ 25000	10.1	20.4	33.3
CaCl ₂ 50000	7.0	17.1	27.7
CaCl ₂ 100000	6.9	17.6	26.6
NaCl 50000	7.0	17.3	28.0
KCl 50000	6.9	17.3	27.3
Filtrate	47.6	79.1	90.6

3 PERMEABILITY REDUCTION

LAS NO. 3047-2

<u>DEPTH = 2072 Feet</u>	<u>TIME</u>		
	<u>15 Min.</u>	<u>30 Min.</u>	<u>One Hour</u>
Fresh Water	60.3	86.4	89.6
CaCl ₂ 25000	14.6	29.4	51.4
CaCl ₂ 50000	10.4	20.6	33.9
CaCl ₂ 100000	10.0	20.1	31.4
NaCl 50000	10.0	20.3	32.0
KCl 50000	10.1	20.0	31.6
Filtrate	50.6	79.7	90.2

<u>DEPTH = 2069 Feet</u>			
Fresh Water	90.6	96.4	98.2
CaCl ₂ 25000	77.3	82.6	88.0
CaCl ₂ 50000	68.0	80.3	82.1
CaCl ₂ 100000	67.7	80.4	80.4
NaCl 50000	67.6	81.0	82.6
KCl 50000	68.1	81.4	82.6
Filtrate	80.6	92.4	96.8

6-X

3 PERMEABILITY REDUCTION

LAB NO. 3047-3

<u>DEPTH = 2066 Feet</u>	<u>TIME</u>		
	<u>15 Min.</u>	<u>30 Min.</u>	<u>One Hour</u>
Fresh Water	50.3	69.9	75.9
CaCl ₂ 25000	14.0	30.6	49.6
CaCl ₂ 50000	11.0	21.3	34.0
CaCl ₂ 100000	10.6	20.0	33.2
NaCl 50000	11.0	20.9	34.3
KCl 50000	10.8	20.9	34.6
Filtrate	42.1	66.6	70.2

LISTING OF OTHER AVAILABLE GEOLOGIC & PERTINENT DATA

1. Final Micropaleontology Reports by Anderson, Warren & Associates, Inc.
 - a. Foraminifera Report, Walakpa No. 1, March 25, 1980.
 - b. Palynology Report, Walakpa No. 1, March 25, 1980.
2. Drilling History Report, Walakpa Test Well No. 1 (prepared by Husky Oil NPR Operations, Inc.).
3. Halliburton Drill-Stem Test Reports with Charts for Drill-Stem Tests No. 1 and No. 2.
4. Analysis of Cased Hole Drill-Stem Test, Walakpa Test Well No. 1, NPRA, by Gruy Management Service Co., March 21, 1980, 5 pages with Appendices.
5. Source of Other Geological & Well Data:

Copies and/or reproducibles of all geological data are available from:

National Oceanic and Atmospheric Administration
EDIS/NGSDC (D62)
325 Broadway
Boulder, CO 80303