

NATIONAL PETROLEUM RESERVE IN ALASKA

GEOLOGICAL REPORT

SOUTH BARROW WELL NO. 19

HUSKY OIL NPR OPERATIONS, INC.  
Prepared by: R. G. Brockway

For the

U. S. GEOLOGICAL SURVEY  
Office of the National Petroleum Reserve in Alaska  
Department of the Interior  
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COMPOSITE LITHOLOGY LOG (In Pocket)

## GEOLOGIC SUMMARY

### INTRODUCTION

The South Barrow Well No. 19, 1320' FEL and 1320' FSL, protracted Section 23, T22N, R17W, Umiat Meridian (Figures 1 & 2), was drilled to define the northern limits of the East Barrow Gas Field. Drilling began below conductor casing at 80' (driller's depth) on April 18, 1978. Rocks of Cretaceous through Triassic age were penetrated. The drilling was terminated at a total depth of 2,300 feet on May 6 in argillite of indeterminate age, and the rig was released on May 16, 1978.

In each of the South Barrow wells drilled after South Barrow No. 13, an inhibitive mud system, containing calcium-chloride, was used after intermediate casing (commonly 9-5/8" to approximately 1,500 feet). This was done in order to minimize damage to potential reservoirs caused by swelling clays, which are present in the Barrow sandstones and the Sag River Sandstone (determined by water susceptibility tests on cores from South Barrow Nos. 12 and 13 wells). The high concentrations of calcium-chloride used in the section below the intermediate casing, necessitated running a dual laterolog, as the high calcium and chloride ion concentration in the drilling mud adversely affects the measurement of conductivity by the dual induction log. The dual induction log was run in the upper part of each well where fresh-water-mud was used.

Five conventional cores were cut and 75 sidewall cores were shot with a recovery of 66. One drill-stem test and one production test were undertaken.

The well was completed as a suspended gas well.

### PRE-DRILLING PROGNOSIS

The primary objective of the well was the Lower Barrow sandstone, with the Sag River Sandstone, thin sandstones in the lower "Pebble Shale", and possibly the Upper Barrow sandstone, as secondary objectives.

### POST-DRILLING SUMMARY

Drilling of Well No. 19 confirmed a northward extension of the East Barrow field and established that it was higher on structure than either of the two correlating wells, South Barrow Wells Nos. 12 and 17. At the top of the Lower Barrow sandstone, Well No. 19 was 17 feet higher than No. 12 and 81 feet higher than No. 17 (Figure 3).

The Lower Barrow sandstone had 17 net feet of porous sandstone with porosities averaging 22% and a water saturation of 40% (Appendix C). This zone was production tested with a calculated absolute open flow of 7.22 MMCFGPD (Appendix H). This establishes this well as the best in the field.

A drill-stem test of the Sag River Sandstone recovered an estimated 800,000 CFGPD and 7 gallons of gassy oil-cut mud from the interval 2161-2245' (Appendix E). Analysis of Core No. 5 (2230-2245') shows porosities of 9.1 to 22.1 and poor to fair permeabilities.

Other secondary objectives ("Pebble Shale" and Upper Barrow) contained hydrocarbon shows, but because of thin bedding, low permeabilities and argillaceous content, they were not deemed worthy of testing.

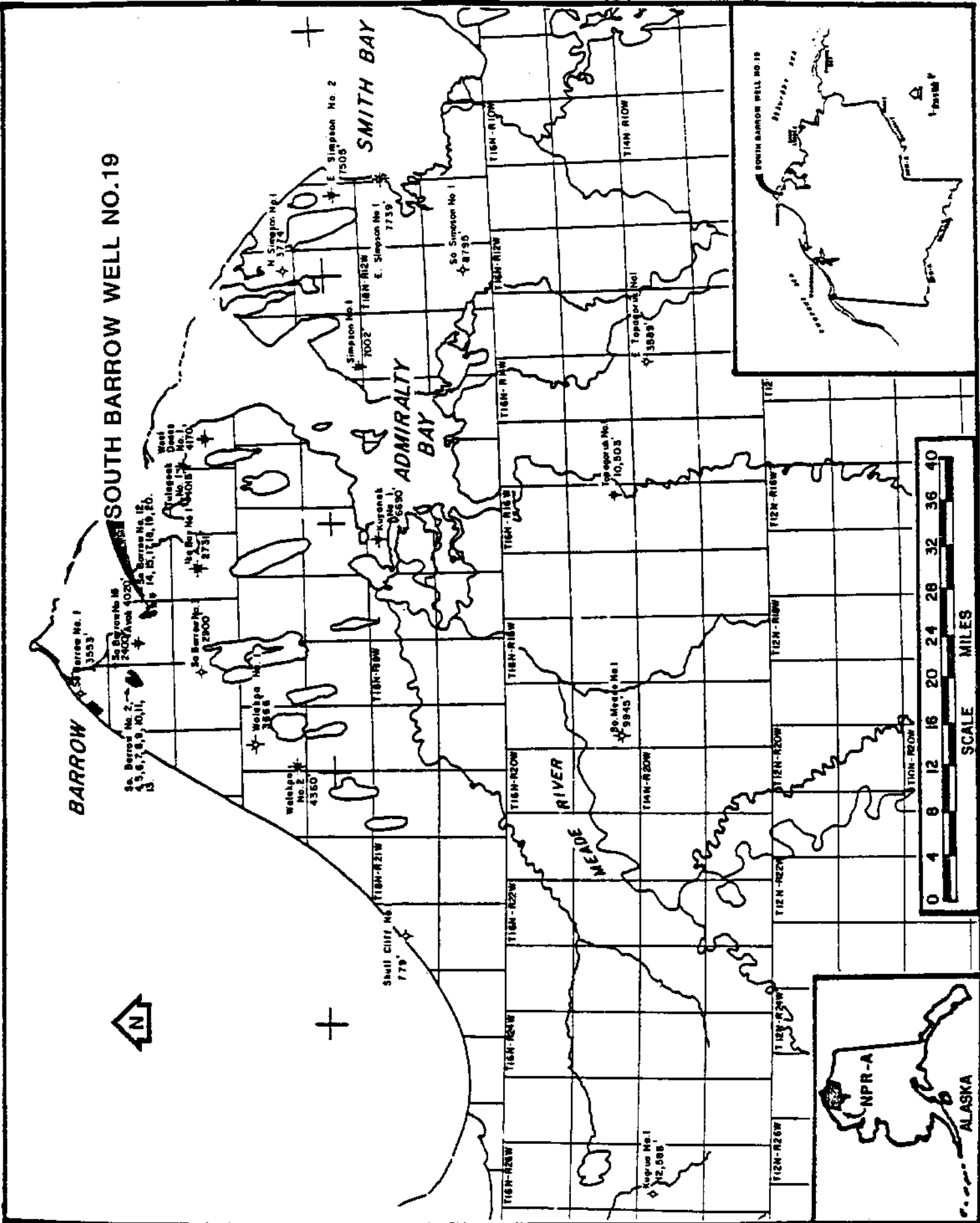
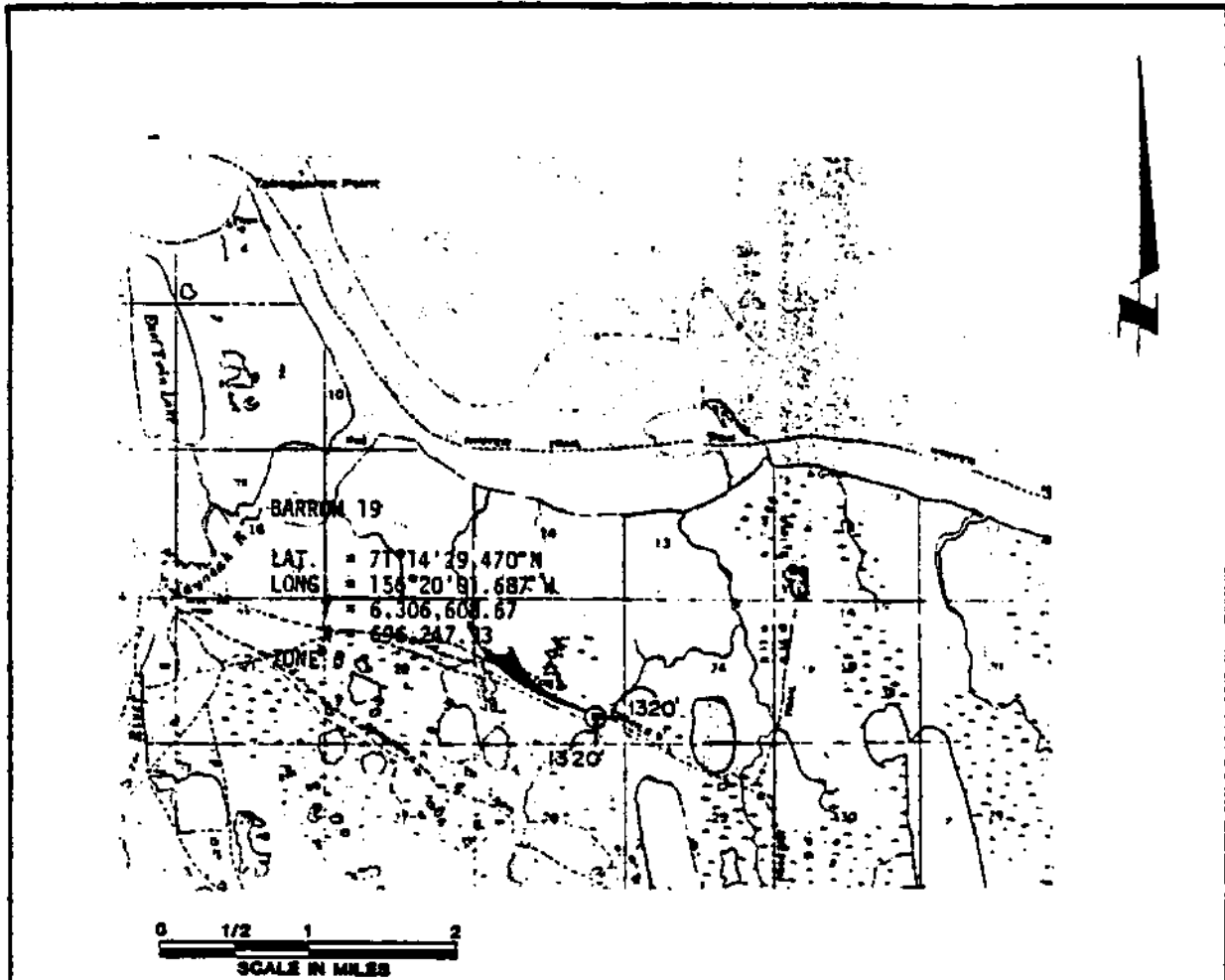


FIGURE 1 - LOCATION MAP - SOUTH BARROW WELL NO. 19



**CERTIFICATE OF SURVEYOR**

I hereby certify that I am properly registered and licensed to practice land surveying in the State of Alaska and that this plat represents a location survey made by me or under my supervision, and that all dimensions and other details are correct.

August 24, 1977



<p>AS STATED  <b>BARROW 19</b>          LOCATED IN  <small>SE 1/4 PROTRACTED SEC. 23 T22 N, R17W UTM MERIDIAN, 48</small>          Surveyed for  <b>HUSKY OIL</b>  <b>N.P.R. OPERATIONS INC.</b></p>
<p>Surveyed by  <b>Bell, Herring and Associates</b>  <b>ENGINEERS AND LAND SURVEYORS</b>          801 West Fireweed, Suite 102          ANCHORAGE, ALASKA 99503</p>

FIGURE 2 - CERTIFICATE OF SURVEYOR - SOUTH BARROW WELL NO. 19

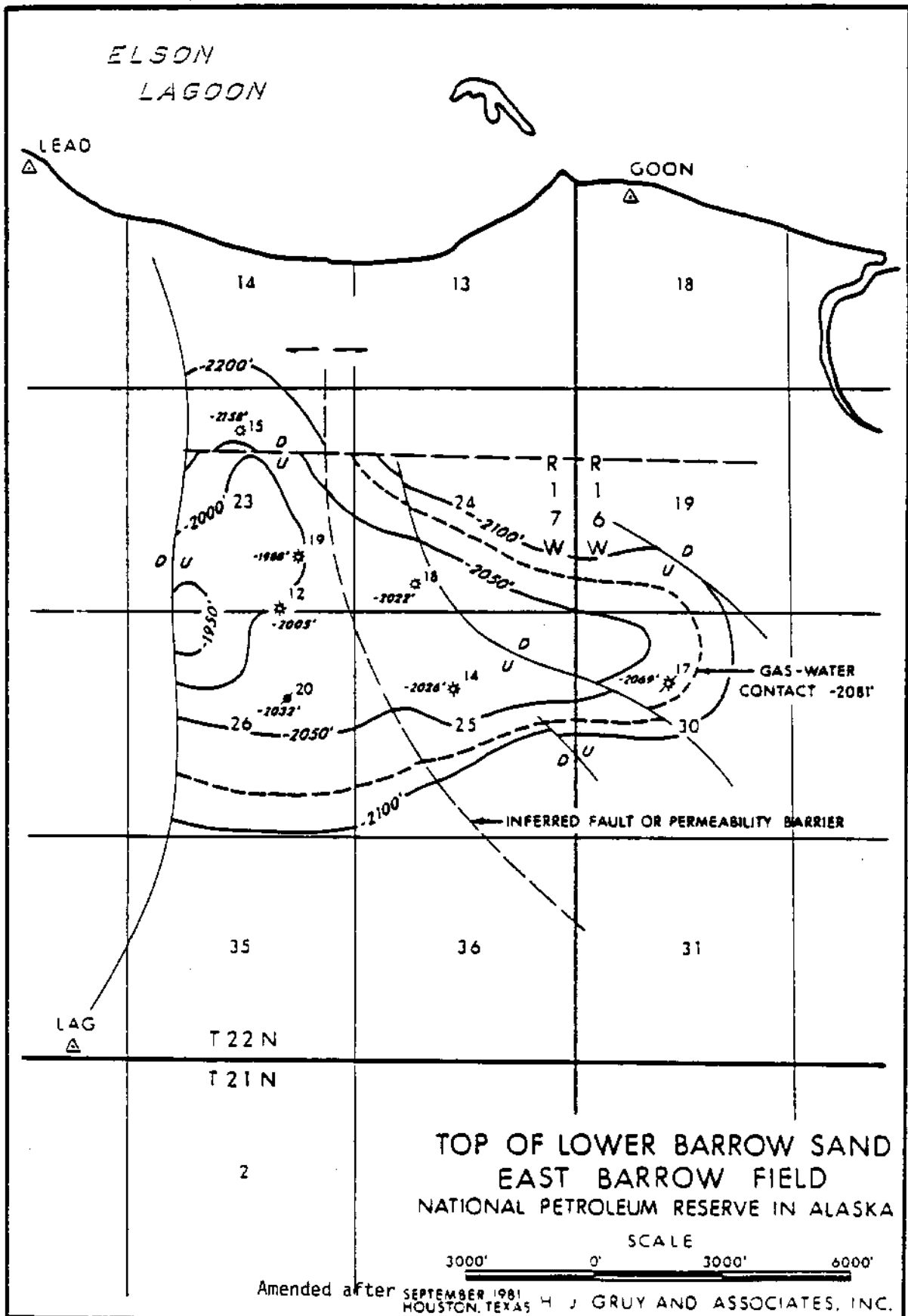


FIGURE 3 - STRUCTURE MAP - SOUTH BARROW WELL NO. 19



WELLSITE GEOLOGIST'S REPORT  
 BY: D. YOUNG  
 REVISED BY: R. G. BROCKWAY

INTRODUCTION

The South Barrow Well No. 19 was drilled as a step-out well to help delineate the northern limit of the East Barrow Gas Field. The Lower Barrow sandstone was the primary objective. Additional objectives were the Sag River Sandstone and the thin persistent sands of the "Pebble Shale". The well was drilled to a total depth of 2,300 feet, penetrating rocks of Cretaceous to Triassic age and terminated in the argillite of indeterminate age. The Lower Barrow sandstone included 17' of net porous sand; it was production tested at a rate of 7.22 MMCFGPD calculated absolute open flow. The "Pebble Shale" sandstone stringers were poorly developed and were not tested. The Sag River Sandstone, with a gross thickness of 54' of shaly sands, was drill-stem tested at an estimated rate of 800 MCFGPD. Gas- and very slightly oil-cut mud were recovered from the test tools. The well was completed as a suspended gas well from the Lower Barrow sandstone.

A total of five conventional cores were cut. Core No. 1 was cut for stratigraphic purposes to help define the Torok-"Pebble Shale" boundary. Cores Nos. 2, 3, 4, and 5 were taken for reservoir purposes. In addition to the conventional cores, 75 sidewall cores were shot with 66 recovered. Drill-bit cuttings were continuously collected from spud to total depth. Sample increments of 30' were used from spud to 1500' and 10' from 1500' to total depth.

STRATIGRAPHY

WIRELINE TOPS

	DRILLED DEPTH (FEET BELOW KELLY BUSHING)	SUBSEA
<b>CRETACEOUS</b>		
Torok Formation	100'	-70'
"Pebble Shale"	samples start 1352'	-1322'
<b>JURASSIC</b>		
Kingak Formation	1744'	-1714'
Upper Barrow sandstone	1952'	-1922'
Lower Barrow sandstone	2018'	-1988'
<b>TRIASSIC</b>		
Undifferentiated	2153'	-2123'
Sag River Sandstone	2194'	-2164'

INDETERMINATE		
Argillite	2264'	-2234'
TOTAL DEPTH	2300'	-2270'

### CRETACEOUS

#### Torok Formation: 100-1352'

Lithology of the Torok consists of interbedded sandstones, siltstones and claystones. The sandstones, most prominent in the upper 370' and lower 150' of the formation, are light gray, fine grained, hard, carbonaceous, argillaceous, calcareous and in part pyritic. A few small gas shows were recorded below 1190'. Siltstones are dark gray, hard and calcareous. The claystones are medium to light gray, soft, sticky, and silty in part. Scattered fossil fragments are present.

The first paleontological age determinations by Anderson, Warren & Associates, Inc. indicate an age of Early Cretaceous, Aptian to Albian, to a depth of 1330'. Faunal diversity and abundance suggest a middle neritic environment of deposition for the interval from 100' to 820'. With species diminishing in diversity and abundance from 820' to 1330', only some type of marine conditions is suggested. No identifiable log correlations exist within the Torok, although faunal correlation points at 160' and 430' appear to be recognizable with South Barrow Wells Nos. 12, 14 and 17.

Bulk lithology for the Torok is approximately 80% claystone, 17% siltstone, and 3% sandstone.

#### "Pebble Shale": 1352-1744'

The top of the "Pebble Shale" is based on a gamma-ray log pick at 1352' and is supported by paleontological age determinations as the boundary between Aptian-Albian and Neocomian age faunas. The boundary was cored with no sharp contact apparent. The contact appears to be at 1350' in Core No. 1 (1330-1360') where medium to dark gray claystones grade to dark gray hard, fissile shales with rare "floaters" of frosted quartz grains. These shales continue downward with an increasing brown color to a depth of 1497'. Some tan to brown limestone was observed in the samples below 1390' (abundant at 1470-1480').

The interval from 1497' to 1645' contains the thin sandstone beds that are found in other Barrow wells in the area. No improvement in thickness or porosity was noted in these sands over those in other wells, although increased gas readings are associated with most of them. The sandstones of this interval are thin bedded (maximum 7') light gray, fine grained, silty and argillaceous. Hydrocarbon fluorescence was noted in the sandstones below 1587'. Interbedded with the sandstones are brown silty shales.

Dark brownish-gray shales with a few thin sandstones occupy the interval 1645-1704'. A chert and quartz pebble conglomerate and fine grained sandstone are present at 1704-1712' (DLL log).

It appears from the electric logs that the zone 1712-1744' may be a transition zone above the lower Cretaceous unconformity. Sidewall cores at 1732' and 1737' recovered black shale with medium to coarse grained and pebble-size quartz and chert. Ditch samples indicate brown shales, dark gray siltstone, and 20-30% loose chert, quartz, and argillite pebbles. A 320-unit gas reading was present from 1740-1745', and it may be that a remnant of the basal "Pebble Shale" conglomerate is present from 1740-1744'. The E-logs indicate a "dirty" sand, conglomerate or siltstone in this interval.

Age of the interval 1680-1740' is determined by Anderson, Warren & Associates, Inc. (Final Micropaleontological Report, July 25, 1978) as Early Cretaceous to Late Jurassic (Neocomian). They note that "this assemblage contains forms suggestive of Late Jurassic but could conceivably still be in Early Cretaceous". Possibly the Jurassic forms are reworked from pre-existing Jurassic rocks cut by the lower Cretaceous unconformity.

The environment of deposition for the "Pebble Shale" is thought to have been neritic to middle bathyal with turbid conditions.

Bulk volume is approximately 77% claystone, 15% siltstone and 8% sandstone.

## JURASSIC

### Kingak Formation: 1744-2153'

The top of the Kingak Formation, which contains the Upper and Lower Barrow sandstones, has been placed at 1744', the base of the transition zone. From 1744' to 1952', the rocks are composed of brownish-gray shales and brown claystones with interbedded light and dark gray siltstones and some thin light gray, fine to very fine grained sandstones.

### Upper Barrow sandstone: 1952-2006'

Sandstones of the Upper Barrow are light gray, very fine grained, glauconitic and argillaceous. Fossil wood and lignite are common. Interbedded with the sandstones are thin siltstones and shales. Poor hydrocarbon shows were observed in the sandstones. Environment of deposition is thought to be shallow marine off bar facies.

The base of the Upper Barrow has been picked at 2006', the base of a thin resistive zone on the DIL or DLL logs and a shale break on the gamma-ray logs that can be correlated throughout the field.

Separating the Upper Barrow from the Lower Barrow is a sandstone and shale sequence. The sandstones are similar to those of the Upper Barrow and have some hydrocarbon shows. At the base of this interval and capping the Lower Barrow sandstone is a thin 1-2' shale that is readily recognized and used as a marker bed on the gamma-ray logs throughout the field.

Lower Barrow sandstone: 2018-2037'

At 2018', a 19' section of porous Lower Barrow sandstone was entered. The sands of the Lower Barrow are interpreted to be central bar facies. The quartz sand is tan to light gray, very fine grained, clean to slightly argillaceous, friable, glauconitic, with occasional lignite and fossil wood fragments. Some swelling clay in the matrix is indicated by swelling and disintegration of samples in fresh water. Sidewall cores indicate claystone pods and partings with poorly preserved crossbedding at 2032'. Large, soft, clayey, dark green glauconite grains were noted in a sidewall core at 2036'. Good hydrocarbon shows were observed and the zone 2018-2044' was production tested at a calculated AOF rate of 7.22 MMCFGPD.

The Kingak Formation below the Lower Barrow from 2037' to 2153', consists of light gray, very fine grained, argillaceous quartz sandstone interbedded with dark gray siltstones and light gray silty claystone.

Core No. 2 (2039-2069') is interbedded light gray, very fine grained, argillaceous sandstone and medium to dark gray siltstone, with common lignite and fossil wood. Swelling clays are indicated by fresh-water tests. A thin bed of pelecypods (species unknown) occurred at 2048'. No dips were apparent from the core and it is thought that bioturbation has removed all evidence of bedding in these strata.

The strata of the Kingak Formation have been assigned an Early to Middle Jurassic age (AWA Zones F-17 to F-18).

Environment of deposition below 2153' to 2250' is thought to have been inner to middle neritic.

TRIASSIC

Undifferentiated: 2153-2194'

A 41' interval of Triassic rocks, identified by paleontology, is present above the Sag River Sandstone. It is composed of thin interbedded tan to light gray, fine to coarse grained sandstones, medium gray siltstones and light gray claystones. The faunal top of the Triassic (AWA Zone F-19 which extends to 2250') was picked at 2153'. No hiatus is apparent in the samples.

Sag River Sandstone: 2194-2264'

The Sag River top was picked on the basis of samples and electric log responses and is marked by a thin bed of limestone that is tan, hard, sandy, and slightly glauconitic. This bed was also noted in South Barrow Well No. 17. The top of the sandstone is thought to be at 2200'. Cores Nos. 3, 4, and 5 (2209-2245') were cut in the Sag River. Lithology of the cores was very fine grained quartz sandstone. The sandstone is brown, well sorted, well rounded, argillaceous, calcareous, with common shell fragments and glauconite. Thin biocalcarenite shell pods (probably echinoid plates and pelecypods) occur at 2219' and 2230-2233'. The limestone is white to tan with viscous oil in intergranular porosity. Thin

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stringers of soft amorphous glauconite and dark gray-brown shale also occur. At 2222', bedding planes of 45° were noted. These are interpreted as probably foreset beds. Minor fracturing was noted at this depth also, being parallel to and at right angles to the bedding planes. Good oil stain is present throughout the Sag River. A much higher percentage of sandstone was noted in the Sag River in this well than in South Barrow No. 17 where sandy biocalcarenite is the predominant lithology.

Drill-Stem Test No. 1 (2161-2245') recovered an estimated 800 MCFGD and 7 gallons of gas- and slightly oil-cut mud.

Lithology from 2245' to the top of the argillite at 2264' consists of light gray, argillaceous, calcareous sandstone with interbedded medium gray, soft claystone.

Environment of deposition for the Sag River is suggested to be inner to middle neritic.

Bulk lithology of the Sag River is approximately 14% shale, 16% limestone, and 70% sandstone.

#### PRE-MISSISSIPPIAN

##### Argillite: 2264-2300' (Total Depth)

The argillite was entered at 2264' with a change in lithology to dark gray-black, firm to hard, slightly graphitic, pyritic argillite. Finely disseminated pyrite, thin quartz lenses, and free quartz are common in the ditch cuttings.

#### STRUCTURE

Core No. 1, 1330-1360', which included the Torok-"Pebble Shale" contact had poorly developed partings in the shale and claystone indicating horizontal bedding with no apparent unconformity.

A Schlumberger 4-arm dipmeter was run over the interval 1500' to 2174' to aid in structural interpretation. Low dip angles ranging from 2° to 4°, trending generally north-northwest, occur from 1550' to 1740'. At the top of the Kingak Formation (1744'), which is considered to be a surface of unconformity, dip increased to a maximum of 8°, averaging 4°, with direction changing from north-northwest to north-northeast.

From 1800' to 2039', dips range from 2° to 5°, averaging 3°, with direction to the north and northeast. A sidewall core at 2032', with poorly preserved crossbedding, indicated low angle bedding on shale partings.

From 2039' to 2080', dip continues at a 3° average with direction changing from north-northeast to south-southwest. No dip information was detectable from Core No. 2, 2039-2069'. Bioturbation probably has removed all evidence of bedding in this interval.

From 2080' to 2170', dips range from 4° to 6°, averaging 5°, with orientation to the west.

A dipmeter was not run in the bottom-hole section of the well due to small hole size. Cores Nos. 3, 4, and 5 were cut over the interval 2209' to 2245'. Low angle dips of approximately 5° are present on shale partings. At 2222', poorly developed 45° foreset bedding was noted.

## OIL AND GAS INDICATIONS

### Torok Formation

Very slight indications of methane gas were noted from the start of logging at 100'. Total gas increased from 2 units at 845', to an average of 40 units to 900' (maximum 80 units) and contained the first occurrence of ethane. Small gas peaks were noted at 1190', 1240', 1290', and 1315' from thin sandstone stringers. These sandstones are generally light gray, fine grained, argillaceous, and hard.

No potential reservoir rock was present in the Torok Formation.

### "Pebble Shale"

A gas reading of 576 units was logged at 1475' to 1480' on the mud log and appears to be associated with a thin limestone which was present in the 1470-1480' samples. Possibly some sandstone is present but was not detected in the samples. The S.P. log indicates a slight amount of porosity at 1476'. Components of the gas were: methane, 10,500 ppm; ethane, 300 ppm; and a trace of propane. A sidewall core cut at 1476' recovered claystone.

From 1587' to 1594', a light gray, fine grained sandstone stringer was cut giving a gas peak of 296 units. Dull yellow-gold sample fluorescence, giving a slow, streaming, yellow cut fluorescence, was observed. Analysis of a sidewall core at 1587' indicated an effective porosity of 23.4% and a permeability of 26 millidarcies.

At 1640' to 1643', another sandstone stringer was penetrated. A gas reading of 960 units was noted with components of 60,000 ppm methane and traces of ethane. The sandstone, light gray and very fine grained, had bright yellow sample fluorescence and an immediate yellow cut fluorescence.

Other thin sands occur at 1660' to 1662'; 1695' to 1697'; and 1710' to 1715'. These sands gave minor gas readings; however, they were more argillaceous than the preceding sands.

### Kingak Formation

Gas peaks of 280 to 390 units occurred at 1940' and 1950', respectively, from thin argillaceous sandstone beds.

The Upper Barrow sandstone was entered at 1952', and below this depth, fairly continuous sandstones occur. Fourteen sidewall cores were recovered from 1952' to 2018'. Lithology of the sidewall cores was predominantly sandstone, generally light gray, very fine grained, argillaceous, poorly consolidated with silt and clay in the matrix. Tests indicate the presence of swelling clays. There was a poor gas odor, and rare dull gold fluorescence with a slight crush cut from chloroethane. Measured porosities from sidewall cores range from 18.8% at 1996' to 26.4% at 1972', with the average being 20.9%. Horizontal permeability ranging from 9.4 millidarcies at 1996' to 273 millidarcies at 1972' were noted. Water saturations are all in excess of 50%. A gas peak of 270 units was noted within this interval.

The Lower Barrow sandstone was picked by log and samples at 2018'. The sandstones become cleaner with less clay and silt content than those above, and have higher effective porosities, lower water saturations, and higher horizontal permeabilities. Porosities range from 17.4% at 2020' to 26.1% at 2034', as measured from sidewall cores. Log-derived porosity averages 21%, with water saturation calculated at 40%. Gross thickness of the pay sand is 19' with 17' of net pay.

At 2020', gas rose from a background of 100 units to a peak of 1,500 units. Gas readings remained at 1,000 units to a depth of 2039', where mud weight was raised from 10.7 ppg to 11.7 ppg prior to coring. The component breakdown of the gas was 92,000 ppm methane, 20,000 ppm ethane, with a trace of propane. Good gas odor, stain, and yellow fluorescence were present in the samples.

The interval directly beneath the porous Lower Barrow sandstone was cored from 2039' to 2069' (Core No. 2). This interval had sample fluorescence, good gas odor, and yellow cut fluorescence. Below 2069' and down to the top of the Sag River Sandstone, no hydrocarbon shows were observed.

The Lower Barrow sandstone was production tested at a calculated absolute open flow rate of 7.22 MMCFGPD. Actual gauging on 29/64" choke was 3.687 MMCFGPD. Additional test information is available in Appendix H.

#### Sag River Sandstone

The Sag River was encountered at 2194'. A very slight increase in gas was noted from 10 units to 20 units. Maximum gas of 200 units was recorded at 2250' in the basal portion of the Sag River. The gas was composed entirely of methane.

Cores Nos. 3, 4, and 5 (2209-2245') were generally bleeding oil and gas with good gas odor. Fractures, with good oil staining on the faces, were present in Core No. 4. Good to spotty gold fluorescence and light brown chloroethane cuts were present throughout the Sag River. At 2230' to 2233', dark brown tarry oil was present in interparticle porosity in a biocalcarenite sequence.

Drill-Stem Test No. 1 was run from the 7" casing shoe at 2161' down to 2245' in the Sag River. A 540 psi nitrogen cushion was used. One flow period of 225 minutes was used with gas to the surface in 23 minutes. Flow rate stabilized at 800 MCFGPD (estimated) through 3/4" choke. Fluid recovery consisted of gas- and very slightly (less than 1%) oil-cut emulsified drilling mud. Pressure charts indicate a low productivity depleting reservoir.

Pressure Data - Bottom Bomb at 2216'

IHP	1,270 psi
IFP	331 psi
FFP	204 psi
ISIP	1,017 psi
FHP	1,220 psi
Temperature	55°F

Argillite

The argillite was entered at 2264'. No hydrocarbon indications were noted from the argillite down to total depth of 2300'.

CONCLUSIONS

1. The complete sedimentary section was penetrated and evaluated at this location.
2. The "Pebble Shale" sandstone stringers appear to be gas bearing; however, clay and silt in the matrix combined with the thinness and probable discontinuity of the beds make significant production unlikely.
3. The well extended the East Barrow Gas Field one location to the north and proved up an additional 17' of structural advantage to the South Barrow No. 12 well.
4. The oil shows in the Sag River are concluded to be noncommercial residual oil. While gas was tested from the Sag River at the rate of 800 MCFGPD, the pressure charts appear to indicate a depleting low productivity reservoir.
5. No hydrocarbon shows were indicated in the argillite.



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SUMMARY OF PERTINENT DATA \*

WELL NAME: South Barrow Well No. 19  
 API NO.: 50-023-20012  
 OPERATOR: Husky Oil NPR Operations, Inc.  
 LOCATION: 1320' FEL, 1320' FSL  
 protracted Section 23, T22N, R17W,  
 Umiat Meridian, Alaska  
 COORDINATES: Latitude: 71°14'29.470"N  
 Longitude: 156°20'01.687"W  
 X = 696,247.93  
 Y = 6,306,608.67  
 Zone 6  
 ELEVATION: 7' Ground, 12' Pad, 30' Kelly Bushing  
 DATE SPUDDED: April 18, 1978  
 TOTAL DEPTH: 2,300 feet  
 2,100 feet - plug-back depth  
 DATE REACHED  
 TOTAL DEPTH: May 6, 1978  
 RIG RELEASED: May 16, 1978  
 STATUS: Gas Well (Suspended)  
 CASING: 13-3/8" @ 80' (driller)  
 9-5/8" @ 1491'  
 7" @ 2161'

LOGGING RECORD:

DIL/SP	99-1495'
DLL/SP/Caliper	1491-2173'
DLL/SP	2161-2284
BHCS/GR/TTI/Caliper	100-1497'
	1490-2170'
	2161-2296'
FDC/CNL/GR/Caliper	1490-2176'
	2062-2294'
FDC/GR/RR/Caliper	1490-2176'
	2062-2294'
MLL	2110-2299'
CBL/VDL/GR	1450-2081'
Mudlog	80-2300'

LOGGING RECORD: (Continued)

Computed Logs:  
Dipmeter Arrow Plot 1501-2167'  
Saraband 1500-2260'

SIDEWALL CORES: Run 1, Shot 30, Recovered 29  
Run 2, Shot 45, Recovered 37

CONVENTIONAL CORES:

<u>No.</u>	<u>Depth</u>	<u>Recovery</u>	<u>Formation</u>
1	1330-1360'	30'	Torok & "Pebble Shale"
2	2039-2069'	30'	Lower Barrow
3	2209-2217'	4'	Sag River Sandstone
4	2217-2230'	9'	Sag River Sandstone
5	2230-2245'	15'	Sag River Sandstone

TESTS:

DST No. 1 2161-2245' 800 MCFGPD (estimated) and 7 gallons gas- and very slightly oil-cut emulsified mud.

Production Test No. 1 perf. 2018-2044' Calculated AOF 7.22 MMCFGPD.

ANALYSIS REPORTS:

Crude Oil: Chemical & Geological Laboratories of Alaska, Inc.  
Gas Analysis: U. S. Bureau of Mines  
Gas Analysis: Chemical & Geological Laboratories of Alaska, Inc.

WELLSITE GEOLOGIST: D. Young

WELL LOG ANALYST: Armour Kane

CONTRACTOR: Brinkerhoff Signal, Inc.

MUD LOGGERS: Borst & Giddens Well Logging Service, Inc.

BIOSTRATIGRAPHIC ANALYSIS: Anderson, Warren & Associates, Inc.

\* Copies and/or reproducibles of all geological data are available from:

National Oceanic and Atmospheric Administration  
EDIS/NGSDC (D62)  
325 Broadway  
Boulder, CO 80303

SOUTH BARROW WELL NO. 19  
DRILL CUTTINGS AND CORE DESCRIPTIONS  
BY: D. YOUNG

DRILLED DEPTH  
(FEET BELOW  
KELLY BUSHING)

0- 100	No recovery.
100- 220	Sandstone: light gray, fine grained, medium hard, silty, carbonaceous, calcareous, argillaceous, interbedded with Siltstone: medium gray, hard, carbonaceous, calcareous, a few pelecypod fragments.
220- 370	Sandstone: fine grained, light to medium gray, hard, calcareous, carbonaceous in part, argillaceous, a few pyritic inclusions.
370- 460	Claystone: gray, soft, sticky.
460- 490	Siltstone: light gray, argillaceous, firm, calcareous.
490- 760	Claystone: medium gray, soft, sticky, slightly silty, with interbedded siltstone and minor sandstone.
760- 820	Siltstone: dark gray, hard, calcareous.
820- 880	Claystone: as above.
880- 940	Claystone: medium gray, soft, sticky, interbedded with Sandstone: fine grained, light gray, hard, calcareous, pyritic.
940-1000	Claystone: medium gray, soft, sticky, interbedded with Siltstone: dark gray, hard, calcareous, pyritic and Sandstone: very fine grained, light gray, hard, calcareous, trace of kaolinite, trace of pelecypods.
1000-1120	Claystone: medium gray, soft, sticky, interbedded with Siltstone: dark gray, calcareous, hard, occasional pyrite, trace of kaolinite.
1120-1180	No sample returns.
1180-1210	Claystone: gray, brown, soft, lumpy, interbedded with Siltstone: dark gray, firm, pyritic, calcareous.
1210-1300	Sandstone: fine grained, hard, light gray, argillaceous, calcareous, pyritic, interbedded with siltstone and Claystone: as above.
1300-1330	Claystone: light gray, soft, sticky.

1330-1360

Core No. 1 - Cut 30', Recovered 30'

1330.0-1335.0' (5.0')	Claystone: medium gray, silty, firm, blocky, faint gassy odor.
1335.0-1338.0' (3.0')	Claystone: medium gray, silty, firm, as above.
1338.0-1340.0' (2.0')	Claystone: medium gray, silty, firm, slightly pyritic, poor gassy odor.
1340.0-1344.0' (4.0')	Claystone: medium to dark gray, firm, slightly silty.
1344.0-1348.0' (4.0')	Claystone: medium to dark gray, firm, hard, slightly silty, becomes fissile, noncalcareous.
1348.0-1350.0' (2.0')	Claystone: grading to dark gray Shale: fissile, noncalcareous, poor horizontal partings.
1350.0-1353.0' (3.0')	Shale: dark gray, hard, fissile, pyritic inclusions, rare Gastropod imprint, probable spines.
1353.0-1356.0' (3.0')	Shale: dark gray, fissile, hard, pyritic inclusions, slickensides common, horizontal partings.
1356.0-1359.0' (3.0')	Shale: dark gray, hard, fissile, as above.
1359.0-1360.0' (1.0')	Shale: as above, few pyritic inclusions, horizontal partings.
1360-1390	Shale: as above, trace of calcite, trace of coal.
1390-1450	Shale: dark gray, fissile, as above, and dark green, glauconitic, interbedded with Limestone: tan to brown, green, pyritic, hard, tight, common frosted quartz grains.
1450-1500	Shale: brown, soft, slightly fissile, calcareous, interbedded with Limestone: tan to brown, pyritic, in part silicified, large pyritohedrons, common loose frosted quartz grains.
1500-1570	Shale: dark brown-gray, soft, silty, occasional pyrite inclusions, and wood fragments, a few loose medium quartz grains.

- 1570-1590 Sandstone: fine grained, light gray, argillaceous, silty, clear, white, brown, green, pyritic, dull yellow-gold fluorescence with slow streaming cut, yellow cut fluorescence, interbedded with Shale: as above.
- 1590-1640 Shale: dark brown, soft, silty, slightly pyritic, becoming micromicaceous with a few loose quartz grains.
- 1640-1650 Sandstone: fine grained, light gray, argillaceous, silty matrix, poorly sorted, subangular, subrounded, clear quartz, 10% dark mafics, dull gold fluorescence, immediate streaming cut, yellow cut fluorescence.
- 1650-1660 Shale: dark brown-gray, silty, soft, micaceous, few rounded frosted quartz grains, trace of pyrite.
- 1660-1670 Sandstone: fine grained, light gray, slightly argillaceous, silty matrix, clear quartz, yellow-gold fluorescence, slight cut.
- 1670-1680 Shale: brown-gray, soft, silty, micaceous, common free frosted quartz grains.
- 1680-1690 Sandstone: as above.
- 1690-1700 Shale: brown, soft, silty.
- 1700-1710 Conglomerate: pebbles of chert, quartz, and argillite, free, subrounded to well rounded, interbedded with Sandstone: fine grained, light gray, tight, hard, argillaceous, poorly sorted, and Siltstone: dark gray, argillaceous, firm.
- 1710-1720 Limestone: brown, argillaceous, hard, tight, abundant siderite(?), orange to clear, partly euhedral, with gold fluorescence, interbedded with common coarse grained to pebble sized free quartz, chert and argillite, well rounded.
- 1720-1740 Shale: brown, soft, highly sandy, abundant loose, fine to medium grained quartz, chert and argillite.
- 1740-1780 Siltstone: dark gray, highly argillaceous, firm with thin beds of Sandstone: fine grained, light gray, friable, argillaceous, glauconitic, calcite common, pebbles, as above.
- 1780-1850 Shale: brown-gray, soft, silty, in part slightly fissile, gradational with claystone.

- 1850-1890 Siltstone: light gray, argillaceous, soft, gradational with Claystone: soft, silty, micromicaceous.
- 1890-1910 Claystone: brown, soft, micaceous.
- 1910-1920 Claystone: as above, interbedded with Siltstone: gray, argillaceous, firm.
- 1920-1930 Siltstone: dark gray, firm, pyrite inclusions with Limestone stringers: brown, hard, dense.
- 1930-1940 Claystone: gray, soft, silty.
- 1940-1950 Siltstone: light gray, soft, highly argillaceous, grading to very fine grained, highly argillaceous sandstone.
- 1950-1970 Sandstone: very fine grained, light gray-tan, glauconitic, hard, argillaceous, pyritic, fossil wood with interbedded Siltstone: brown, soft, highly argillaceous, highly sandy, slightly calcareous.
- 1970-1980 Sandstone: very fine grained, light gray, tan, friable, silty matrix, micaceous, slightly argillaceous, glauconitic, no odor, stain, or fluorescence.
- 1980-1990 Sandstone: very fine grained, light gray, tan, silty, argillaceous, friable, clay matrix, common fossil wood and lignite, glauconite, clear, white, green quartz, a few orange pebbles.
- 1990-2000 Sandstone: as above, very slight gas odor, poor yellow crush cut, yellow cut fluorescence.
- 2000-2020 Sandstone: very fine grained, light gray, silty matrix, slightly argillaceous, fossilized wood, slight odor of gas, dull gold fluorescence, slight crushed cut, yellow cut fluorescence, in part tan, hard, slightly calcareous.
- 2020-2030 Sandstone: very fine to fine grained, clean, clear, very friable, loose grained, subrounded to rounded, well sorted, quartzose, clear, white, 5% dark green, gold fluorescence, 100% yellow cut fluorescence.
- 2030-2039 Sandstone: very fine grained, light gray, tan, friable, clean, clear, trace of light green quartz, large dark green glauconite, abundant loose sand grains, gold fluorescence, slight stain, slight yellow cut, in part clay filled matrix.

2039.0-2042.0' (3.0')	Sandstone: fine grained, tan, firm, friable, slightly silty, clay in matrix, swells on test with fresh water, clear quartz, well sorted, subrounded to rounded, bright yellow, mottled fluorescence, immediate yellow cut, yellow cut fluorescence.
2042.0-2045.0' (3.0')	Sandstone: fine grained, tan, silty, swelling clay in matrix, friable, glauconite, as above, lignite, pelecypod, megafossils.
2045.0-2047.0' (2.0')	Sandstone: fine grained, tan to light gray, silty clay in matrix, calcareous.
2047.0-2047.2' (0.2')	Sandstone: fine grained, tan to light gray, argillaceous, clear, hard; Siltstone: argillaceous, hard, sandy, calcareous, yellow fluorescence, good cut.
2047.2-2048.0' (0.8')	Siltstone: argillaceous, hard, sandy, calcareous, yellow fluorescence, good cut.
2048.0-2049.0' (1.0')	Siltstone: firm, medium gray, highly argillaceous, shell bed, small pelecypod, lignite.
2049.0-2051.5' (2.5')	Siltstone: dark gray, firm, sandy, pyritic, bioturbation.
2051.5-2054.0' (2.5')	Sandstone: very fine grained, tan to gray, argillaceous, silty, firm, poorly friable, spotty fluorescence, yellow cut.
2054.0-2056.0' (2.0')	Sandstone: very fine, gray, tan, light gray, silty, argillaceous, calcareous, pyritic.
2056.0-2058.1' (2.1')	Siltstone: dark gray, sandy, calcareous, yellow spotty fluorescence, good odor, fair yellow cut fluorescence, large fossil wood fragment, 5" x 2".



2058.1-2059.0' (0.9')	Sandstone: very fine grained, highly argillaceous, silty, clay pods.
2059.0-2060.0' (1.0')	Sandstone: as above.
2060.0-2061.0' (1.0')	Sandstone: as above, highly argillaceous, silty, good odor.
2061.0-2062.0' (1.0')	Sandstone: light gray, very hard, siliceous, pyritized fossil wood.
2062.0-2063.0' (1.0')	Sandstone: very fine grained, light gray, partly clean and fine grained, good odor, yellow fluorescence, yellow cut fluorescence.
2063.0-2066.0' (3.0')	Sandstone: light gray, very fine grained, hard, argillaceous, calcareous.
2066.0-2069.0' (3.0')	Sandstone: light gray to brown, very fine grained, hard, argillaceous, silty, slightly friable, spotty yellow fluorescence, good gassy odor.
2069-2080	Sandstone: light gray, very fine grained, slightly argillaceous, few pyritic inclusions, clay matrix swells, with thin beds of dark gray, firm, slightly sandy shale.
2080-2110	Siltstone: dark gray, firm, sandy, interbedded with Sandstone: light gray to tan, hard, tight, highly calcareous, and Shale: gray, slightly fissile, firm.
2110-2140	Siltstone: dark gray, firm, slightly sandy, micaceous, slightly calcareous, with thin stringers of Sandstone: fine grained, tan, hard, partly friable, clear, subrounded, quartzose.
2140-2170	Claystone: light gray, soft, highly sandy.
2170-2175	Sandstone: tan to light gray, fine grained, hard, subrounded to rounded, clear, white quartz, glauconitic, interbedded with Claystone: as above.
2175-2180	Siltstone: medium gray, firm, calcareous, slightly carbonaceous, micromicaceous.

- 2180-2185 Sandstone: medium to coarse grained, angular quartz, light gray, argillaceous, calcareous, slightly carbonaceous, Siltstone: as above.
- 2185-2190 Siltstone, as at 2175', trace of brown oil stain with gold fluorescence.
- 2190-2195 Limestone: tan, hard, sandy, slightly glauconitic, orange, gold fluorescence, very slight cut.
- 2195-2205 Sandstone: fine grained, brown to tan, argillaceous, calcareous, a few coarse grained pebbles, rounded quartz grains as floaters with thin bed of Claystone: light gray, firm, abundant gilsonite.
- 2205-2209 Sandstone: fine grained, tan to brown, light gray, slightly argillaceous, hard, tight, common glauconite, subrounded, clear quartz, a few quartz pebbles, 10% gold fluorescence, gold cut fluorescence.
- 2209-2217 Core No. 3 - Cut 8', Recovered 4'
- 2209.0-2209.7' Shale: dark gray, very hard, carbonaceous, slightly silty.  
(0.7')
- 2209.7-2211.0' Sandstone: very fine to fine grained, brown, firm to slightly friable, highly glauconitic, subrounded to well rounded quartz, good brown oil stain, tea cut, 100% gold fluorescence, shell fragments of pelecypod and echinoid.  
(1.3')
- 2211.0-2212.0' Sandstone: very fine grained, brown, very friable, glauconite, quartz, as above, poorly consolidated, silty matrix, good brown oil stain, fluorescence cut, bleeding oil, in part good visible porosity.  
(1.0')
- 2212.0-2213.0' Sandstone: very fine grained, brown to gray, friable, glauconite, highly argillaceous, clay in matrix.  
(1.0')
- 2213.0-2217.0' No recovery.  
(4.0')
- 2217-2230 Core No. 4 - Cut 13', Recovered 9'
- 2217.0-2219.3' Sandstone: very fine grained, brown, clean, highly glauconitic,  
(2.3')

thin beds, well sorted, well rounded quartz, few pelecypod shell fragments, slightly calcareous.

2219.3-2220.2'  
(0.9') Limestone: brown to tan, firm, biocalcarenitic, sandy, highly glauconitic beds, calcareous.

2220.2-2222.0'  
(1.8') Sandstone: brown, very fine grained, firm, glauconitic.

2222.0-2223.0'  
(1.0') Sandstone: very fine grained, brown, poorly consolidated, very friable, argillaceous, clear, well rounded, well sorted quartz, glauconitic, heavy oil stain, 45° bedding planes, vertical fractures and fractures at right angles to bedding planes possibly induced, closed to slightly open good stain on faces, no mineralization.

2223.0-2225.0'  
(2.0') Sandstone: as above at 2220.2', highly calcareous, increase in fossils with pelecypod and echinoid plates.

2225.0-2226.0'  
(1.0') Sandstone: very fine grained, brown, friable, highly calcareous, highly glauconitic, pelecypods and echinoids, clean, clear, well rounded quartz.

2226.0-2230.0'  
(4.0') No recovery.

2230-2245

Core No. 5 - Cut 15', Recovered 15'

2230.0-2231.2'  
(1.2') Limestone: white, tan-brown, hard, fossils, glauconitic, sandy, spotty oil stain, gold fluorescence 100%, scattered, dense, black tar blebs, pelecypod and echinoid fragments, thin shale and sandstone partings; Shale: dark gray-brown, hard, gold spores, Sandstone: stringers, very fine grained, friable, firm, brown, glauconitic, heavy oil stain, tea cut.

2231.2-2232.8'  
(1.6') Limestone: biocalcarenite, white, clear, tan, green, large shell fragments, common pelecypod,

	echinoid plates, large glauconitic pellets, soft amorphous, few small argillaceous pebbles, dark brown, high visible crude in pockets of porosity, good odor, spotty stain.
2232.8-2236.0' (3.2')	Sandstone: very fine grained, brown, calcareous, hard, good odor and oil stain, slightly friable, scattered shell fragments, bleeding oil and gas.
2236.0-2238.0' (2.0')	Sandstone: as above, very hard, siliceous, good fluorescence, poor stain.
2238.0-2240.0' (2.0')	Sandstone: very fine grained, brown, calcareous, hard, low porosity, poor permeability, 100% gold fluorescence, tea cut, pelecypod, brachiopod, scattered shells.
2240.0-2243.0' (3.0')	Sandstone: very fine grained, brown, well sorted, well rounded, slightly friable, calcareous, shell fragments, rare glauconite, slightly argillaceous, good odor, stain cut fluorescence, bleeding oil and gas.
2243.0-2245.0' (2.0')	Sandstone: as above, increasingly argillaceous.
2245-2250	Sandstone: very fine grained, light gray, firm, calcareous, argillaceous.
2250-2260	Claystone: medium gray, soft, bedded with Sandstone: as above.
2260-2280	Argillite: dark gray to black, firm, slightly graphitic, flaky.
2280-2290	Argillite: medium to dark gray, firm, graphitic, pyritic, common clear, broken quartz, probably as lenses and fracture fillings.
2290-2300	Argillite: dark gray, firm, graphitic, poorly foliated, in part mottled, light gray, quartzose, common free Quartz: as above; no odor, stain, cut, or fluorescence observed.
2,300 feet Total Depth	

## ARMOUR KANE

Well Log Analyst  
 18360-6 Cantara St  
 Reseda, Ca. 91335  
 (213) 993-0586  
 May 12, 1978

Mr. Gordon W. Legg  
 Husky Oil/NPR Operations, Inc.  
 2525 C Street, Suite 400  
 Anchorage, Alaska 99503

Dear Mr. Legg:

Logging operations on South Barrow #19 were begun by Schlumberger at 1300 hours April 30, 1978 and completed at 0400 hours May 1. Logs run were Dual Laterolog, Neutron-Density, Sonic, Dipmeter and sidewall cores. The DLL had to be run twice due to SP trouble, the Neutron-Density had to be run twice due to "spikes" on the neutron curve, the caliper was inoperative on the sonic log and their sepia print paper was too old to print. In my opinion, these problems and those on other wells show a disturbing lack of preventative maintenance on Schlumberger's part.

Log tops were: Kingak, 1714; Upper Barrow Sand, 1965; Lower Barrow Sand, 2018. The Upper Barrow appears quite shaly and of low permeability while the Lower Barrow indicates an average porosity of 22%, an average water saturation of 40% and invasion diameter of 30-35 inches. It should produce gas with some water cut.

The final logging run was commenced at 1300 hours May 6 and was completed at about 2300 hours May 7, 1978. Trouble was encountered with the DLL resulting in some 6 hours of lost rig time, the Neutron-Density and Sonic logs were run successfully, one more try with the DLL was a failure and the Microlaterolog failed to reach bottom. A cleanout run was made and after replacement equipment was flown in the DLL was completed. However, the field printer broke down so field prints of the DLL and MLL could not be obtained. Again, a maintenance problem.

The Sag River Sand was topped at 2194 and Argillite at 2264. Sag River porosity averaged 15% and water saturation 48%. Here, again,  $R_w$  values were 0.12 to 0.13, or about 50,000 ppm as in Barrow #17 compared to measured values of produced water in #17 of .45 to .49. A check of Barrow #12, drilled with fresh mud, resulted in a computed  $R_w$  of 0.5 and average porosity of 23% and water saturation of 48%, which compares favorably with the figures from Barrow #17 and #19. True resistivity in #12 was from 30 to 38 ohm-meters and in #19 from 13 to 20 ohms. This is a problem difficult to resolve but it would appear that log interpretation can be relied upon as borne out by well performance in #17.

Very truly yours,



Armour Kane

# Log Analysis

COMPANY HUSKY OIL/NPR OPERATIONS, INC.						WELL SOUTH BARROW #19			
FIELD SOUTH BARROW			COUNTY NORTH SLOPE			STATE ALASKA			

DEPTH	RT	Φ <sub>D</sub>	Φ <sub>N</sub>	ΔT	Φ <sub>S</sub>	* Φ <sub>SC</sub>	Φ <sub>C</sub>	Sw	DI	REMARKS	
2018-20	13	21	24	100	30	21	21	46	30°		
2020-22	13	27	21	105	33	23.1	25	38	30°		
2022-26	18	27	21	108	36	25.2	25	33	32°		
2026-30	20	15	27	102	32	22.4	15	52	33°		
2030-34	18	26	23	108	36	25.2	25	33	33°		
2034-36	18	22	25	110	37	25.9	22	37	35°		
					Av. Φ = 22%						
					Av. Sw = 40%						
<p>R<sub>MF</sub> = .012 @ 61° BHT EST = 70° R<sub>MF</sub> @ 70° = .063</p> <p>R<sub>MF</sub> = .036 SP @ 2030 = 25 MH</p> <p><math>\frac{R_{MF}}{R_w} = .42</math> R<sub>w</sub> = .085 R<sub>w</sub> = DI2 = 6900 ppm</p>											
* Φ <sub>S</sub> CORRECTED FOR GAS EFFECT BY "RULE OF THUMB" FIGURE OF 0.7											



# Log Analysis

COMPANY HUSKY OIL/NPR OPERATIONS, INC. WELL SOUTH BARRROW #19  
 FIELD SOUTH BARRROW COUNTY NORTH SLOPE STATE ALASKA

DEPTH	R <sub>F</sub>	D <sub>0</sub>	D <sub>1</sub>	CAT #10 ΔT	Φ <sub>s</sub>	Φ <sub>c</sub>	Φ <sub>e</sub>	S <sub>w</sub>		Φ <sub>FF</sub>	S <sub>w</sub> X FT.	REMARKS
2018-20	13	21	24	100	30	21	21	46		42	92	
2020-22	13	27	21	105	33	23.1	25	38		50	76	
2022-26	18	27	21	108	36	25.2	25	33		100	122	
2026-30	20	15	27	102	32	22.4	15	52		60	208	
2030-34	18	26	23	108	36	25.2	25	33		100	122	
2034-36	18	22	25	110	37	25.9	22	37		44	74	
										296	716	
										A <sub>v</sub> Φ = 22	40%	
Φ <sub>s</sub> CORRECTED FOR GAS EFFECT BY "RULE OF THUMB" FIGURE OF 0.7												

R<sub>MF</sub> = .092 @ 61° ESTIMATED BHT = 70°  
 R<sub>MF</sub> @ 70° = .063 R<sub>ME</sub> = .036 SP @ 2030 = + 25' AV.  
 R<sub>MS</sub> = .42 R<sub>WC</sub> = .085 R<sub>w</sub> = .12 = 60,000 ppm  
 R<sub>c</sub>





# CHEMICAL & GEOLOGICAL LABORATORIES OF ALASKA, INC.

TELEPHONE (907) 279-4014

P.O. BOX 4-1276

4649 Business Park Blvd.

ANCHORAGE, ALASKA 99509

## CORE ANALYSIS REPORT

Company Husky Oil Company Date May 3, 1978 Lab. No. 7818  
 Well No. South Barrow No. 19 Location \_\_\_\_\_  
 Field NPR No. 4 Formation \_\_\_\_\_  
 County \_\_\_\_\_ Depths Core No. 2 (2039-2069)  
 State Alaska Drilling Fluid \_\_\_\_\_

**LEGEND**  
 C—Crack  
 F—Fracture  
 H—Horizontal  
 O—Open  
 NF—No Fracture  
 IS—Insufficient Sample  
 S—Slight  
 St—Stain  
 V—Vertical  
 Vs—Vugs

SAMPLE NO.	LEGEND	DEPTH, FEET	EFFECTIVE POROSITY PERCENT	PERMEABILITY MILLIDARREYS		SATURATIONS		CORRATE WATER	SOLUBILITY	
				HORIZONTAL	VERTICAL	% PORE SPACE RESIDUAL OIL	% PORE SPACE TOTAL WATER		H2S ACID	IS % ACID
1.		2039-40	14.1	3.35	2.13	Trace	69.4			
2.		2040-41	18.9	61	6.88	5.6	68.2			
3.		2041-42	22.2	83	67	5.4	58.0			
4.		2042-43	2.0	5.75	4.40	1.9	80.2			
5.	HF	2043-44	8.6	91	7.11	2.1	81.7			
6.		2044-45	13.9	14	8.55	7.1	50.0			
7.		2045-46	16.9	8.91	10	Trace	57.9			
8.		2046-47	14.3	24	20	Trace	60.6			
9.		2047-48	14.3	2.30	0.84	Trace	57.4			
10.		2048-49	13.7	2.06	2.00	Trace	69.7			
11.		2049-50	14.8	1.27	0.63	Trace	58.6			
12.		2050-51	13.6	2.12	1.07	Trace	62.1			
13.		2051-52	17.7	5.56	2.26	1.4	62.8			
14.		2052-53	19.9	12	1.37	1.2	53.6			
15.		2053-54	24.9	4.67	1.55	2.0	56.4			
16.		2054-55	16.4	3.43	1.60	4.5	66.4			
17.		2055-56	18.4	9.91	1.69	2.7	58.3			
18.		2056-57	20.0	11	4.19	2.5	58.9			
19.		2057-58	12.6	5.64	3.03	3.1	71.1			
20.		2058-59	11.6	9.38	4.12	Trace	76.0			
21.		2059-60	18.0	15	10	1.3	62.9			
22.		2060-61	20.8	11	1.94	2.4	51.3			
23.		2061-62	11.1	9.59	0.36	Trace	60.4			
24.		2062-63	17.1	4.40	2.49	Trace	59.8			
25.	HF	2063-64	14.1	40	0.51	Trace	60.1			
26.		2064-65	15.0	6.34	0.42	4.9	59.3			
27.		2065-66	12.6	3.52	1.18	Trace	62.8			
28.		2066-67	14.1	5.96	0.51	5.1	67.7			
29.		2067-68	16.6	1.91	1.19	5.9	61.5			
30.		2068-69	16.0	6.69	3.23	6.1	59.6			



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4649 Business Park Bl.

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CORE ANALYSIS REPORT

Company Husky Oil Company Date May 8, 1978 Lab. No. 7856  
 Well No. South Barrow No. 19 Location \_\_\_\_\_  
 Field NPR #4 Formation \_\_\_\_\_  
 County \_\_\_\_\_ Depths \_\_\_\_\_  
 State Alaska Drilling Fluid \_\_\_\_\_

LEGEND  
 C—Crack  
 F—Fracture  
 H—Horizontal  
 O—Open  
 NF—No Fracture  
 IS—Insufficient Sample  
 S—Slight  
 St—Stain  
 V—Vertical  
 Vu—Vugs

SAMPLE NO.	LEGEND	DEPTH, FEET	EFFECTIVE POROSITY PERCENT	PERMEABILITY MILLIDARCIES		SATURATIONS		CONNATE WATER	SOLUBILITY	
				HORIZONTAL	VERTICAL	% PORE SPACE RESIDUAL OIL	% PORE SPACE TOTAL WATER		H2S ACID	HCl ACID
<u>SIDEWALL CORES</u>										
1.		1587	23.4	26		---	---			
2.		1636	----	--		Trace	63.6			
3.		1960	20.5	33		---	---			
4.		1964	----	--		Trace	55.3			
5.		1972	26.4	273		---	---			
6.		1976	----	--		1.1	54.6			
7.		1980	19.2	18		---	---			
8.		1984	----	--		1.3	58.8			
9.		1988	21.3	20		---	---			
10.		1992	----	--		Trace	60.1			
11.		1996	18.8	9.44		---	---			
12.		2000	----	--		Trace	55.6			
13.		2004	20.6	28		---	---			
14.		2014	----	--		Trace	52.1			
15.		2016	19.3	17		---	---			
16.		2018	----	--		1.6	40.9			
17.		2020	17.4	14		---	---			
18.		2022	----	--		1.0	42.2			
19.		2024	25.6	58		---	---			
20.		2026	----	--		Trace	40.3			
21.		2028	23.0	43		---	---			
22.		2032	----	--		Trace	41.7			
23.		2034	26.1	26		---	---			
24.		2036	----	--		Trace	48.3			

NOTES: AVERAGE POROSITY OF FOOTAGE ABOVE AND BELOW USED FOR FLUID SATURATIONS.



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CORE ANALYSIS REPORT

Company Husky Oil Company Date May 10, 1978 Lab. No. 7882  
 Well No. South Barrow No. 19 Location \_\_\_\_\_  
 Field NPR #4 Formation \_\_\_\_\_  
 County \_\_\_\_\_ Depths 2230-2245 (Core No. 5)  
 State Alaska Drilling Fluid \_\_\_\_\_

**LEGEND**  
 C—Crack  
 F—Fracture  
 H—Horizontal  
 O—Open  
 NF—No Fracture  
 IS—Insufficient Sample  
 S—Slight  
 St—Stale  
 V—Vertical  
 Va—Vugs

SAMPLE NO.	LEGEND	DEPTH, FEET	EFFECTIVE POROSITY PERCENT	PERMEABILITY MILLIDARREYS		SATURATIONS		CONNATE WATER	SOLUBILITY	
				HORIZONTAL	VERTICAL	% PORE SPACE RESIDUAL OIL	% PORE SPACE TOTAL WATER		H2S ACID	HCl ACID
1.		2230-31	9.1	9.31	0.62	Trace	44.0			
2.		2231-32	16.9	977	712	8.6	52.9			
3.		2232-33	11.7	17.3	2.40	Trace	50.9			
4.		2233-34	15.0	9.13	38.4	Trace	50.0			
5.		2234-35	18.6	19.7	7.28	Trace	55.5			
6.		2235-36	14.7	9.13	7.77	1.8	50.2			
7.		2236-37	13.7	7.18	8.68	3.8	48.7			
8.		2237-38	15.9	15.6	8.31	Trace	47.9			
9.		2238-39	16.3	7.35	4.16	Trace	54.1			
10.		2239-40	13.3	4.38	0.13	3.9	58.4			
11.		2240-41	17.1	38.0	11.8	3.0	53.4			
12.		2241-42	15.1	16.5	12.7	0.9	55.6			
13.		2242-43	17.4	16.4	9.04	Trace	50.5			
14.		2243-44	22.1	82.8	24.8	1.2	48.1			
15.		2244-45	20.2	29.2	13.8	1.3	47.5			



DRILL STEM TEST REPORT FORM

WELL NAME SOUTH BARROW No. 19

Test Number 1 Hole Size 5 5/8" rathole 7" casing

Date 5/5/78 Drill Pipe (Size & Lgth) \_\_\_\_\_

Test Interval 2161-2245' Sag River Drill Collars (Size & Lgth) \_\_\_\_\_  
Top Sag River (2200)

Total Depth 2245' Type of Cushion Fluid Nitrogen gas

Amount of Cushion 540 psi Nitrogen cushion

TEST DATA

1. Tool open at 0607 hours.
2. Initial open period 223 mins.
3. Initial shut-in period ~~367~~ 367 mins.
4. Final flow period not run mins.
5. Final shut-in period not run mins.
6. Description of blow on initial open period Open tool- bled nitrogen cushion 540 psi decr. to 0 psi 0611 ; mod. blow incr to strong ; drill mud to surf. 0618 20 psi
7. Description of blow during test GTS 0630 57 psi; 0800 67 psi stabilized on #2/64 choke; 0843 64 psi stab. on 1/2" chk.; 0950 39 psi stab. on 3/4" chk.
8. G.T.S. 23 mins; 20 O.T.S. \_\_\_\_\_ mins; Bottom hole choke size 3/4"  
Surface choke size variable 20/64, 1/2 3/4
9. Flow Rate: Gas 800 W (estd) C.F.P.D. Oil \_\_\_\_\_ B.P.H. G.O.R. \_\_\_\_\_
10. Gravity of Gas \_\_\_\_\_ Gravity of Oil \_\_\_\_\_
11. Total fluid recovery: 7 gal. from collar below circulating valve and 1 pint  
from sealed sub below tester valve gas and v. slightly oil cut emulsified mud
12. Resistivity of H<sub>2</sub>O \_\_\_\_\_ Chlorides of H<sub>2</sub>O rat hole mud 70,000 ppm P.P.M.
13. Depth of top press bomb 2111 Bottom Bomb 2216

PRESSURE DATE

Depth packer 2129'

Top Bomb: No. <u>7581</u> 24 hour clock	Bottom Bomb: <u>7582</u> 24 hour clock
I.H.P. <u>1224</u>	I.H.P. <u>1270</u>
I.S.I.P. <u><del>995</del> 995</u>	I.S.I.P. <u>1017</u>
I.F.P. <u>333</u>	I.F.P. <u>331</u>
F.F.P. <u>179</u>	F.F.P. <u>204</u>
F.S.I.P. _____	F.S.I.P. _____
F.H.H. <u>1199</u>	F.H.H. <u>1220</u>
Temp. <u>55</u>	Temp. <u>55</u>

SAMPLE CHAMBER DATA

1. Gas \_\_\_\_\_ C.F.
2. Oil \_\_\_\_\_ C.C.
3. H<sub>2</sub>O \_\_\_\_\_ C.C.
4. Mud \_\_\_\_\_ C.C.
5. B.O.R. \_\_\_\_\_ F S. & W. \_\_\_\_\_ %

REMARKS:

4 gas pressure bottles were filled two at 1 hour into test and two at 3 hours 20 min.

4 1 qt. plastic sample containers and 2 1 gal. paint cans were filled with fluid recovery.

DST chart shows a mechanically successful test . Chart interpretation indicates a tight low productivity reservoir based primarily on flow curve analysis.

The sealed sub contained primarily gas at 1000 psi, approx. 1 pint of gas and v. sli. oil cut mud was also recovered.

D. B. Young



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## GAS ANALYSIS REPORT

Company Husky Oil Company Date May 15, 1978 Lab. No. 7868-1  
 Well No. South Barrow No. 19 Location \_\_\_\_\_  
 Field \_\_\_\_\_ Formation Sag River  
 County \_\_\_\_\_ Depth DST No. 1 (2161-2245)  
 State Alaska Sampling point Choke Manifold  
 Line pressure \_\_\_\_\_ psig; Sample pressure 65 psig; Temperature \_\_\_\_\_ ° F; Container number \_\_\_\_\_  
 Remarks Sample No. 1. One hour sample in part drilling mud, 5-5-78.

Component	Mole % or Volume %	Gallons per MCF
Oxygen .....	0	
Nitrogen .....	6.25	
Carbon dioxide .....	0.20	
Hydrogen sulfide .....	---	
Methane .....	91.47	
Ethane .....	1.64	0.055
Propane .....	0.20	0.010
Iso-butane .....	0.03	0.025
N-butane .....	0.08	0.011
Iso-pentane .....	0.03	0.011
N-pentane .....	0.03	0.016
Hexanes .....	0.04	0.014
Heptanes & higher .....	0.03	
Total .....	100.00	0.142
GPM of pentanes & higher fraction .....		0.052
Gross btu cu. ft. @ 60° F. & 14.7 psia (dry basis) .....	967	
Specific gravity (calculated from analysis) .....		0.596
Specific gravity (measured) .....		0.598

Remarks: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_



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## GAS ANALYSIS REPORT

Company Husky Oil Company Date May 15, 1978 Lab. No. 7868-2  
 Well No. South Barrow No. 19 Location Sag River  
 Field NPR #4 Formation Sag River  
 County \_\_\_\_\_ Depth DST No. 1 (2161-2245)  
 State Alaska Sampling point Choke Manifold  
 Line pressure \_\_\_\_\_ psig; Sample pressure 39 psig; Temperature \_\_\_\_\_ ° F; Container number \_\_\_\_\_  
 Remarks Sample No. 2, 3 hour 20 min. sample, 5-5-78

Component	Mole % or Volume %	Gallons per MCF
Oxygen	0	
Nitrogen	6.20	
Carbon dioxide	0.17	
Hydrogen sulfide	---	
Methane	91.44	
Ethane	1.58	0.063
Propane	0.23	0.013
Iso-butane	0.04	0.041
N-butane	0.13	0.015
Iso-pentane	0.04	0.029
N-pentane	0.08	0.021
Hexanes	0.05	0.018
Heptanes & higher	0.04	
Total	100.00	0.200
GPM of pentanes & higher fraction		0.065
Gross btu cu. ft. @ 60° F. & 14.7 psia (dry basis)		972
Specific gravity (calculated from analysis)		0.598
Specific gravity (measured)		0.600

Remarks: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_



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## GAS ANALYSIS REPORT

Company Husky Oil Company Date May 15, 1978 Lab. No. 7863-3  
 Well No. South Barrow No. 19 Location \_\_\_\_\_  
 Field NPR #4 Formation Sag River  
 County \_\_\_\_\_ Depth DST No. 1 (2161-2245)  
 State Alaska Sampling point Choke Manifold  
 Line pressure \_\_\_\_\_ psig; Sample pressure 39 psig; Temperature \_\_\_\_\_ ° F; Container number \_\_\_\_\_  
 Remarks Sample No. 3, 3 hour 20 min. sample, 5-5-78

Component	Mole % or Volume %	Gallons per MCF
Oxygen	0	
Nitrogen	6.23	
Carbon dioxide	0.18	
Hydrogen sulfide	---	
Methane	91.45	
Ethane	1.52	0.060
Propane	0.22	0.013
Iso-butane	0.04	0.041
N-butane	0.13	0.018
Iso-pentane	0.05	0.029
N-pentane	0.08	0.021
Hexanes	0.05	0.023
Heptanes & higher	0.05	
Total	100.00	0.205
GPM of pentanes & higher fraction		0.091
Gross btu cu. ft. @60° F. & 14.7 psia (dry basis)		972
Specific gravity (calculated from analysis)		0.599
Specific gravity (measured)		0.600

Remarks: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_



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## GAS ANALYSIS REPORT

Company Husky Oil Company Date May 18, 1978 Lab. No. 7936-1  
 Well No. South Barrow No. 19 Location \_\_\_\_\_  
 Field NPR #4 Formation Barrow Sand  
 County \_\_\_\_\_ Depth 2018-44  
 State Alaska Sampling point Separator  
 Line pressure \_\_\_\_\_ psig; Sample pressure 260 psig; Temperature 84 ° F; Container number \_\_\_\_\_  
 Remarks Sample No. 1 taken 5-12-78

Component	Mole % or Volume %	Gallons per MCF
Oxygen	0	
Nitrogen	11.65	
Carbon dioxide	0.06	
Hydrogen sulfide	---	
Methane	87.67	
Ethane	0.35	0.022
Propane	0.08	0.003
Iso-butane	0.01	0.035
N-butane	0.11	0.022
Iso-pentane	0.06	0.004
N-pentane	0.01	---
Hexanes & Higher	Trace	---
Total	100.00	0.086
GPM of pentanes & higher fraction		0.026
Gross btu cu. ft. @60° F. & 14.7 psia (dry basis)		900
Specific gravity (calculated from analysis)		0.608
Specific gravity (measured)		0.610

Remarks: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_





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## GAS ANALYSIS REPORT

Company Husky Oil Company Date May 18, 1978 Lab. No. 7936-2  
 Well No. South Barrow No. 19 Location \_\_\_\_\_  
 Field NPR #4 Formation Barrow Sand  
 County \_\_\_\_\_ Depth 2018-44  
 State Alaska Sampling point Separator  
 Line pressure \_\_\_\_\_ psig; Sample pressure 260 psig; Temperature 84 ° F; Container number \_\_\_\_\_  
 Remarks Sample No. 2 taken 5-12-78

Component	Mole % or Volume %	Gallons per MCF
Oxygen	0	
Nitrogen	11.60	
Carbon dioxide	0.06	
Hydrogen sulfide	---	
Methane	87.76	
Ethane	0.33	0.019
Propane	0.07	0.003
Iso-butane	0.01	0.031
N-butane	0.10	0.022
Iso-pentane	0.06	0.004
N-pentane	0.01	---
Hexanes & Higher	Trace	---
Total	100.00	0.079
GPM of pentanes & higher fraction		0.026
Gross btu cu. ft. @60° F. & 14.7 psia (dry basis)	900	
Specific gravity (calculated from analysis)	0.607	
Specific gravity (measured)	0.608	

Remarks: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_



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**GAS ANALYSIS REPORT**

Company Husky Oil Company Date May 18, 1978 Lab. No. 7936-3  
 Well No. South Barrow No. 19 Location \_\_\_\_\_  
 Field NPR #4 Formation Barrow Sand  
 County \_\_\_\_\_ Depth 2018-44  
 State Alaska Sampling point Separator (Fourth Rate)  
 Line pressure \_\_\_\_\_ psig; Sample pressure 270 psig; Temperature 75 ° F; Container number \_\_\_\_\_  
 Remarks Sample No. 3 taken 5-13-78

Component	Mole % or Volume %	Gallons per MCF
Oxygen .....	0	
Nitrogen .....	12.35	
Carbon dioxide .....	0.09	
Hydrogen sulfide .....	---	
Methane .....	86.95	
Ethane .....	0.39	0.014
Propane .....	0.05	0.007
Iso-butane .....	0.02	0.028
N-butane .....	0.09	0.018
Iso-pentane .....	0.05	0.004
N-pentane .....	0.01	---
Hexanes & Higher .....	Trace	---
Total .....	100.00	0.071

GPM of pentanes & higher fraction .....	0.022
Gross btu cu. ft. @ 60° F. & 14.7 psia (dry basis) .....	892
Specific gravity (calculated from analysis) .....	0.611
Specific gravity (measured) .....	0.611

Remarks: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_



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## GAS ANALYSIS REPORT

Company Husky Oil Company Date May 18, 1978 Lab. No. 7936-4  
 Well No. South Barrow No. 19 Location \_\_\_\_\_  
 Field NPR #4 Formation Barrow Sand  
 County \_\_\_\_\_ Depth 2018-44  
 State Alaska Sampling point Separator (Fourth Rate)  
 Line pressure \_\_\_\_\_ psig; Sample pressure 270 psig; Temperature 75 ° F; Container number \_\_\_\_\_  
 Remarks Sample No. 4 taken 5-13-78

Component	Mole % or Volume %	Gallons per MCF
Oxygen .....	0	
Nitrogen .....	12.39	
Carbon dioxide .....	0.09	
Hydrogen sulfide .....	---	
Methane .....	86.88	
Ethane .....	0.41	0.014
Propane .....	0.05	0.007
Iso-butane .....	0.02	0.031
N-butane .....	0.10	0.018
Iso-pentane .....	0.05	0.004
N-pentane .....	0.01	---
Hexanes & Higher .....	Trace	---
Total .....	100.00	0.074

GPM of pentanes & higher fraction .....	0.022
Gross btu cu. ft. @ 60° F. & 14.7 psia (dry basis) .....	892
Specific gravity (calculated from analysis) .....	0.611
Specific gravity (measured) .....	0.613

Remarks: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_







*E. Barrow # 19*

REPORT OF ANALYSIS

F. S. - 15889      M.S.N-67890    H 1.11      OBS. PRES. 60.9      CAL. PRES. 65.6

STATE- ALASKA      COUNTY- NORTHWESTERN

FIELD-BARROW E      WELL NAME- WELL NO. 19

LOCATION- NOT GIVEN *1320' FEL, 1320 FSL*      OWNER- HUSKY OIL NPR OPERATIONS INC  
*SEC. 23, T22N, R. 17W*

DATE COMPLETED- NOT GIVEN *16 MAY, 1978*      DATE SAMPLED- 01/17/80

SAMPLED BY- NICHOLLS & CRANE

NAME OF PRODUCING FORMATION- NOT GIVEN *BARROW SAND*

DEPTH IN FEET-NOT GIVEN *12050*      THICKNESS IN FEET- NOT GIVEN *20'*

SHUT IN WELLHEAD PRES. PSIG- 1000      OPEN FLOW, MCF/D- NOT GIVEN *7,220 MCFAD*

CHECK OF DATA-  
 THE WELL DATA ARE ACCURATE. ( ) WITHOUT CORRECTION. ( ) AS CORRECTED ABOVE.

REMARKS-

ANALYSIS-

METHANE	86.1 %	NORMAL PENTANE	TRACE %	OXYGEN	0.0 %
ETHANE	0.5 %	ISOPENTANE	0.1 %	ARGON	TRACE %
PROPANE	TRACE %	CYCLOPENTANE	TRACE %	HYDROGEN	0.0 %
NORMAL BUTANE	0.1 %	HEXANES PLUS	TRACE %	H2S *	0.0 %
ISOBUTANE	0.0 %	NITROGEN	11.8 %	CO2	0.1 %
SPECIFIC GRAV 0.604				HELIUM	1.22 %
				TOTAL	99.90 %

CALCULATED GROSS BTU/CU. FT., DRY AT 60 DEG. F AND 30 IN. MERCURY- 889  
 \* DUE TO THE ABSORPTION OF H2S DURING SAMPLING, THE REPORTED RESULTS MAY NOT BE RELIABLE

PERMISSION FOR RELEASE:

Permission is hereby granted for the Bureau of Mines to release the above data, together with similar data released by other operators as public information and as parts of a series of papers on analyses of gases from various fields, states, or regions.

COMPANY *U.S. Geological Survey*  
 BY *Robert J. Fane*  
 TITLE *Geologist*



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## CRUDE OIL ANALYSIS REPORT

Company Husky Oil Company Date May 17, 1978 Lab. No. 7870  
 Well No. South Barrow No. 19 Location \_\_\_\_\_  
 Field NPR #4 Formation \_\_\_\_\_  
 County \_\_\_\_\_ Depth DST No. 1  
 State Alaska Analyzed by JP

### GENERAL CHARACTERISTICS

Specific gravity @ 60/60 °F.....	0.9154
A.P.I. gravity @ 60 °F.....	23.1
Saybolt Universal Viscosity @ 70°F., seconds	458
Saybolt Universal Viscosity @ 100°F., seconds	216
B. s. and water, % by volume.....	92
Pour point, °F.....	13
Total sulphur, % by weight.....	1.33

### REMARKS:

\_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

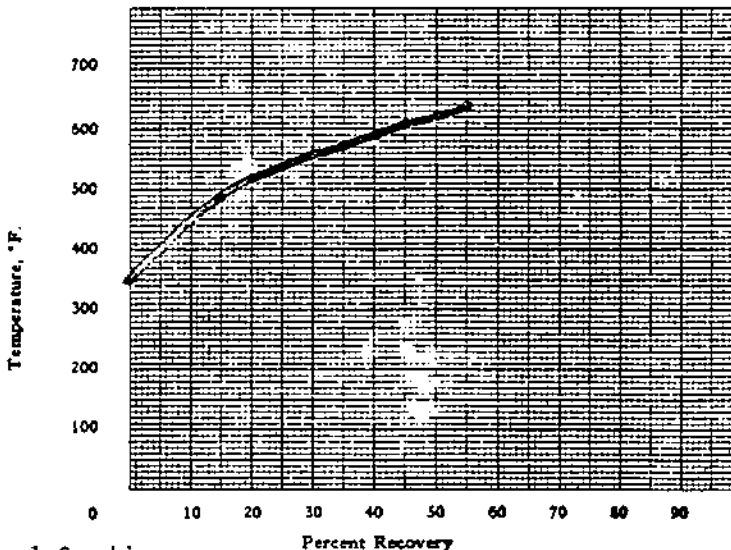
### ENGLER DISTILLATION

Recovery, %	Temperature, °F.
IBP	350
5	398
10	450
15	490
20	518
25	540
30	560
35	576
40	592
45	610
50	624
55	638
60	
65	
70	
75	
80	
85	
90	
95	

E.P. 638-Thermal Cracking

Recovery, % 58.0  
 Residue, % 42.0  
 Loss, % 0

### DISTILLATION GRAPH



### Approximate Recovery

300 EP gasoline, % 0  
 392 EP gasoline, % 4.0  
 500 EP distillate, % 13.0





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**WATER ANALYSIS REPORT**

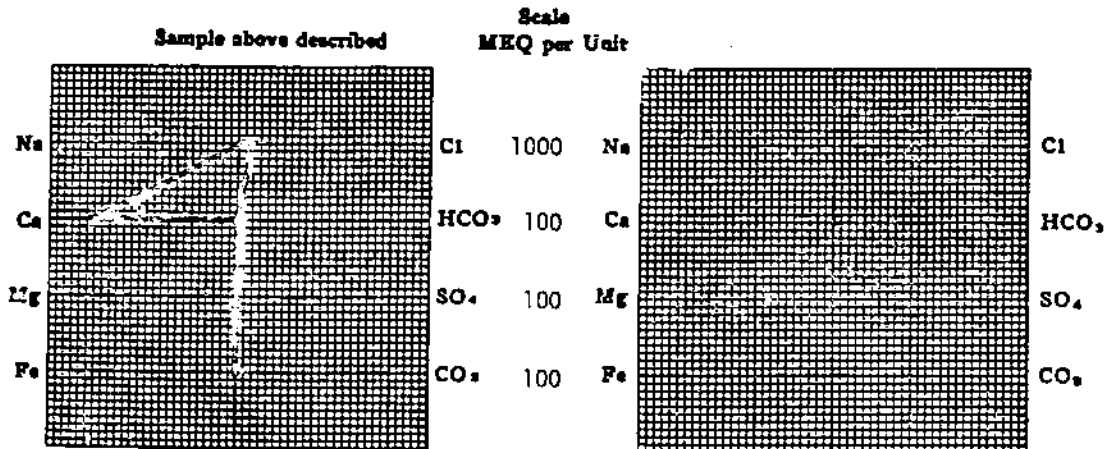
OPERATOR Husky Oil Company DATE May 17, 1978 LAB NO. 7870  
 WELL NO. South Barrow No. 19 LOCATION \_\_\_\_\_  
 FIELD NPR #4 FORMATION \_\_\_\_\_  
 COUNTY \_\_\_\_\_ INTERVAL DST No. 1  
 STATE Alaska SAMPLE FROM \_\_\_\_\_

REMARKS & CONCLUSIONS: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

Cations			Anions		
	mg/l	meq/l		mg/l	meq/l
Sodium	1771	77.07	Sulfate	250	5.20
Potassium	1100	28.16	Chloride	72500	2044.50
Calcium	39000	1946.10	Carbonate	0	---
Magnesium	40	3.29	Bicarbonate	300	4.92
Iron			Hydride	-	---
Total Cations		2054.62	Total Anions		2054.62

Total dissolved solids, mg/l	114809	Specific resistance @ 25°C:	
NaCl equivalent, mg/l	112707	Observed	0.08 ohm-centimeters
Observed pH	7.6	Calculated	0.08 ohm-centimeters

**WATER ANALYSIS PATTERN**



(No value in above graphs includes Na, K, and Li)  
 NOTE: Mg/l = Milligrams per liter Meq/l = Milligram equivalent per liter  
 Sodium chloride equivalent by Dupont & Hawthorne calculation from composition

ENGINEERING MEMORANDA

SOUTH BARROW WELL NO. 19

PRODUCTION TEST NO. I

May 11-14, 1978

This memoranda is a presentation of the reservoir data gathered and reservoir calculations from the production test of the Barrow Sand in the South Barrow Well No. 19. Table I presents basic well and formation data. Table II is a listing of primary analysis results. These are original gas in place, back-pressure analysis, drawdown analysis, pressure buildup analysis, and pressure gradient test analysis. Presented next is a discussion of each analysis. Conclusions and recommendations are followed by data, graphs, and example calculations.

TABLE I - WELL AND FORMATION DATA

1. Barrow Sandstone, early-middle Jurassic	
2. Perforations 2018 to 2044 feet at 4 spf	
3. Gross sand thickness	l = 26 feet
4. Net pay thickness	h = 16 feet
5. Bulk porosity in net pay	$\phi_B = 24.2\%$
6. Effective porosity in net pay	$\phi_e = 20.8\%$
7. Average water saturation in net pay	$S_w = 48.2$
8. Gas gravity	$\rho_g = 0.611$
9. Critical temperature	$T_c = 336.1^\circ R$
10. Critical pressure	$P_c = 650.9 \text{ psia}$
11. Reservoir temperature	$T_i = 527^\circ R$
12. Initial reservoir pressure	$P_i = 984.0$
13. Initial gas compressibility	$Z_i = 0.88$

TABLE II - LISTING OF TEST RESULTS

A. Volumetric Reserves:

Original gas in place = 353.466 McF/AcFt

B. Backpressure Analysis:

Absolute open flow = AOF = 7.22 MMcf/D  
 Back pressure slope = n = 0.844  
 Back pressure constant = C =  $\frac{.000064062 \text{ MMcf/D}}{\text{PSI}^2}$

C. Pressure Buildup Analysis:

Initial reservoir pressure  $P_i = 984 \text{ psia}$   
 Flow Capacity  $kh = 542.19 \text{ md ft}$

Permeability	k = 33.89 md
Skin	S = 1.348
Skin pressure drop	$\Delta P_s = 42.22$ psi
Productivity index (actual)	$J_a = 14.13 \frac{\text{McF/d}}{\text{psi}}$
Productivity index (ideal)	$J_i = 16.87 \frac{\text{McF/d}}{\text{psi}}$
Flow efficiency	Ef = .837
Gas mobility	M = 2854.6 md/cp
Effective wellbore radius	$r_w' = 1.104$ inch
Approximate radius of investigation	$r_{inv} = 462$ ft

D. Wellbore Pressure Gradient Survey:

BHP at 2037 ft	= 980.9
Fluid level	= 1767
WHP	= 793.0
Fluid gradient	= .515 psi/ft

DISCUSSION OF DATA, ANALYSIS TECHNIQUE, AND RESULTS

Original Gas in Place

The porosity, water saturation, and reservoir temperature used in the calculation of Original Gas in Place were derived from log analysis and are representative of the 16 feet of net pay selected between 2023 and 2040 feet. The initial reservoir pressure was derived from the buildup analysis, with both the initial and final buildup curves indicating 984.0 psia. The pressure readings were taken from the Sperry Sun Tool No. 311 at 2037 feet.

The calculated value of Original Gas in Place is 353.466 McF/Ac ft. This is 18.5% higher than the assumed value of 298.2 McF/Ac ft in use for the South Barrow field. The primary cause of this difference is the porosity of 20.8% as opposed to the 16.0% in use as an average field porosity.

Four Point Backpressure Analysis

The pressure-flow history obtained during the four point flow test was very smooth and provided excellent alignment of points in the plot of  $P_c^2 - P_t^2$  vs Q. The indicated absolute open flow was 7.22 McF/d. The backpressure slope was 0.844.

Reservoir Parameter Analysis

Two types of reservoir parameter analysis were performed. The first drawdown of the four point flow was analyzed as was the final buildup. Table III compares the results of these two analyses.

The drawdown analysis technique was based on the semilog plot of Pwf vs log Tp and the pressure equation:

$$P_{wf} = P_i - \frac{28984 q \mu g B_g}{kh} \left[ \log T_p + \log \frac{k}{\phi \mu g C_c r_w^2} - 3.2275 + 0.86859 S \right]$$

The final buildup was analyzed using a multiple flow rate technique with the

$$\text{plot of } P_{ws} \text{ vs } \sum_{j=1}^n \frac{q_j}{q_n} \log \left( \frac{T_n - T_{j-1} + \Delta T}{T_n - T_j + \Delta T} \right)$$

and the equation of the straight line being

$$P_{ws} = P_j - \frac{28984 q \mu g Bg}{kh} \sum_{j=1}^n \frac{q_j}{q_n} \log \left( \frac{T_n - T_{j-1} + \Delta T}{T_n - T_j + \Delta T} \right)$$

This analysis was chosen as the most representative of the reservoir as the flow and buildup times were the longest and the shut in pressure at the start of the flow period was nearest to the projected initial reservoir pressures. Table III shows that the values of kh are in close agreement. The kh in use in the South Barrow field is 154.5 md ft. The calculated kh for Wells No. 14 and No. 17 were 346.28 md ft and 493.80 md ft respectively. The values of Skin,  $\Delta P_s$  and  $r_w'$  show considerable divergence. This can be explained, however, by the rate dependent nature of these parameters. The most significant fact about the Skin and Flow Efficiency parameters is that they show a considerably larger amount of formation damage than was indicated by the tests of Well No. 17 and Well No. 14.

TABLE III - COMPARISON OF TEST ANALYSES

<u>Derived Parameter</u>	<u>Drawdown Value</u>	<u>Buildup Value</u>
Flow Capacity	kh = 567.90 md/ft	kh = 542.19 md/ft
Permeability	k = 35.49 md	k = 33.89 md
Skin	S = .786	S = 1.348
Skin Pressure Drop	$\Delta P_s$ = 6.77 psi	$\Delta P_s$ = 42.22 psi
Actual Productivity Index	$J_a$ = 19.57	$J_a$ = 14.13
Ideal Productivity Index	$J_i$ = 22.06	$J_i$ = 16.87
Flow Efficiency	$E_f$ = 88.71	$E_f$ = 83.7
Gas Mobility	M = 2936.9 $\frac{md}{cp}$	M = 2854.6 $\frac{md}{cp}$
Effective Wellbore Radius	$r_w'$ = 1.936 inch	$r_w'$ = 1.104 inch
Radius of Investigation	$r_{inv}$ = 222 ft	$r_{inv}$ = 462.6 ft

Pressure Gradient Survey

The pressure gradient survey was run with stops at 25, 50, 100, 500, 1000, and 1500 feet of bottom. The survey results are presented in Table II.

### CONCLUSIONS AND RECOMMENDATIONS

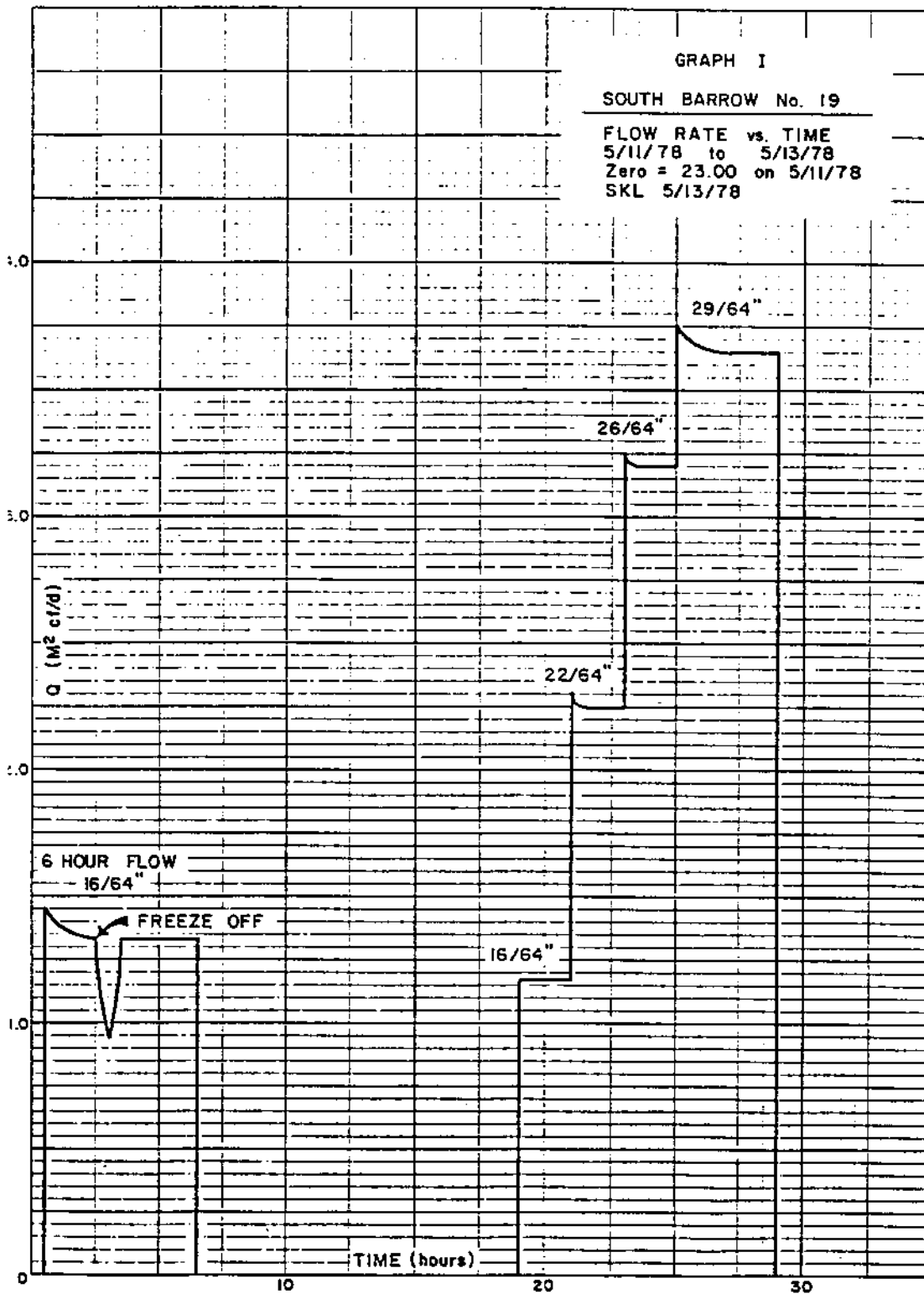
The production testing of South Barrow No. 19 was exceptionally smooth operationally and yielded excellent pressure and flow data. Minor problems were experienced with the test tree and one flow line freeze off was successfully countered with alcohol injection.

The somewhat higher (as compared to South Barrow Wells No. 14 and 17) skin damage may be due to the 232 psi overbalance being carried when the well was perforated. It would appear that 100 psi overbalance might be a better operation parameter from a reservoir viewpoint. Also of interest is the total absence of produced water during the flow period. This is probably due to the structurally high position of the well. As compared to the water production experienced in Well No. 17, the dry nature of Well No. 19 confirms the importance of staying high on the structure in future wells and exercising caution in selecting the perforation interval in any wells which may be drilled lower on the structure.

### DATA AND EXAMPLE CALCULATIONS

Attached are data displays and calculations as listed below.

- |     |                         |  |
|-----|-------------------------|--|
| 1.  | Graph I                 | Flow Rate vs Time  |
| 2.  | Example Calculation I   | Original Gas in Place  |
| 3.  | Graph II                | $P_c^2 - P_t^2$ vs Q   |
| 4.  | Example Calculation II  | Backpressure Data  |
| 5.  | Graph III               | $P_t$ vs Log $T_p$   |
| 6.  | Example Calculation III | Drawdown Analysis  |
| 7.  | Graph IV                | $P_{ws}$ vs $\sum_{j=1}^n q_j / q_n \log \left( \frac{T_n - T_{j-1} + \Delta T}{T_n - T_j + \Delta T} \right)$ |
| 8.  | Example Calculation IV  | Buildup Analysis   |
| 9.  | Graph V                 | $P_{ws}$ vs Depth  |
| 10. | Example Calculation V   | Gradient Analysis  |



EXAMPLE CALCULATION I

Volumetric Reserve Calculation

Original Gas in Place - McF/AcFt

$$43560 \text{ Ft}^2/\text{Ac}$$

$$\phi_e = 20.8\%$$

$$S_w = 48.2\%$$

$$P_i = 984.0 \text{ psia}$$

$$T_i = 67^\circ\text{F}$$

$$z_i = .880$$

$$T_{sc} = 520^\circ\text{R}$$

$$P_{sc} = 14.65 \text{ psia}$$

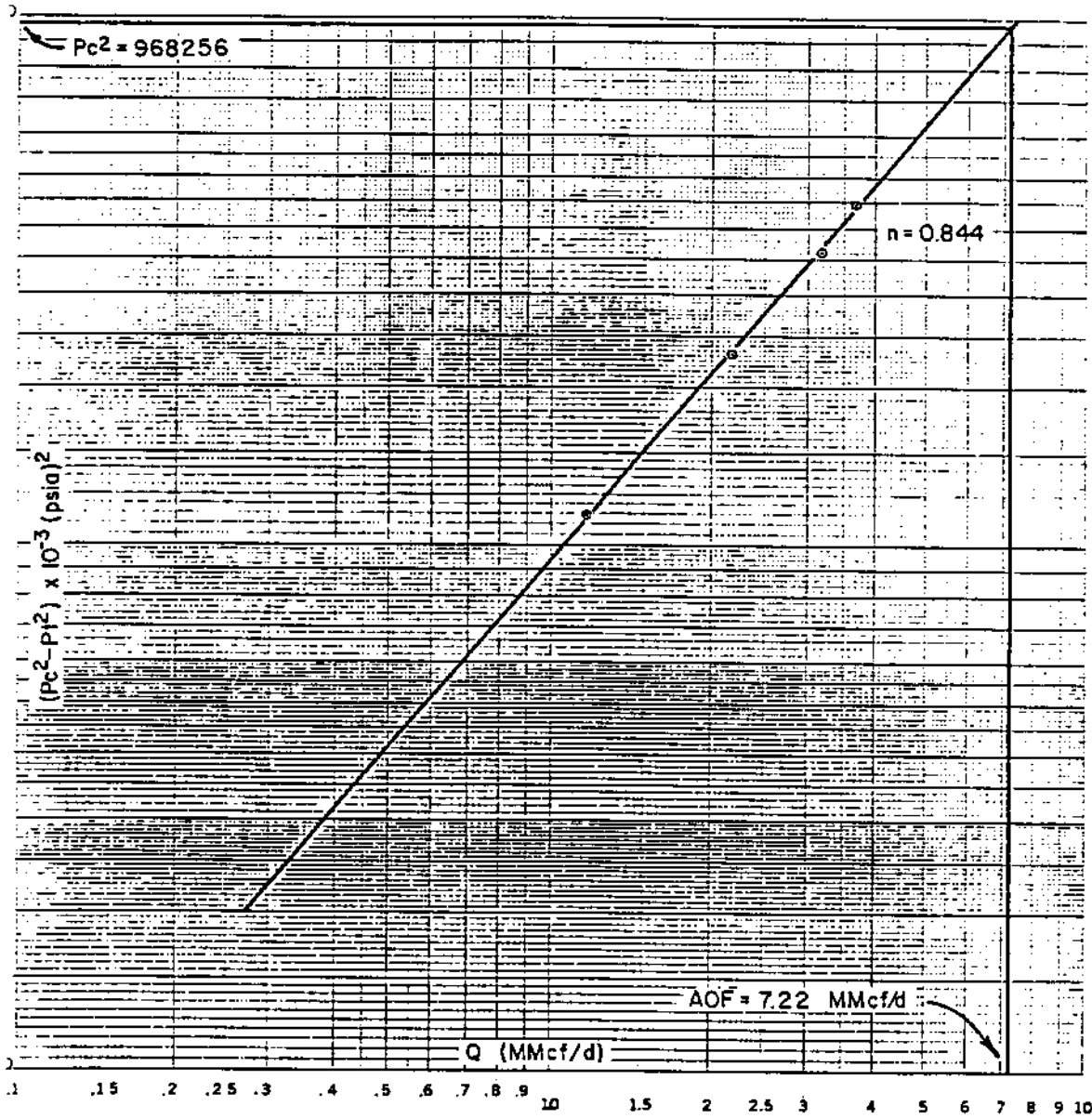
$$\text{OGIP} = A \phi S_g \frac{P_i}{P_{sc}} \frac{T_{sc}}{T_i} \frac{1}{z_i}$$

$$= 43560 \times .208 \times .518 \times \frac{984}{14.65} \times \frac{520}{527} \times \frac{1}{.87}$$

$$= 353.466 \text{ McF/Ac Ft}$$

ATTACHMENT 2

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GRAPH II  
 SOUTH BARROW No. 19  
 Q vs  $Pc^2 - P_1^2$   
 Sperry Sun Tool No. 311  
 at 2037'  
 SKL 5/13/78



EXAMPLE CALCULATION II

Four Point Flow Test - 5/12/78

Initial Reservoir Pressure = 984 psia

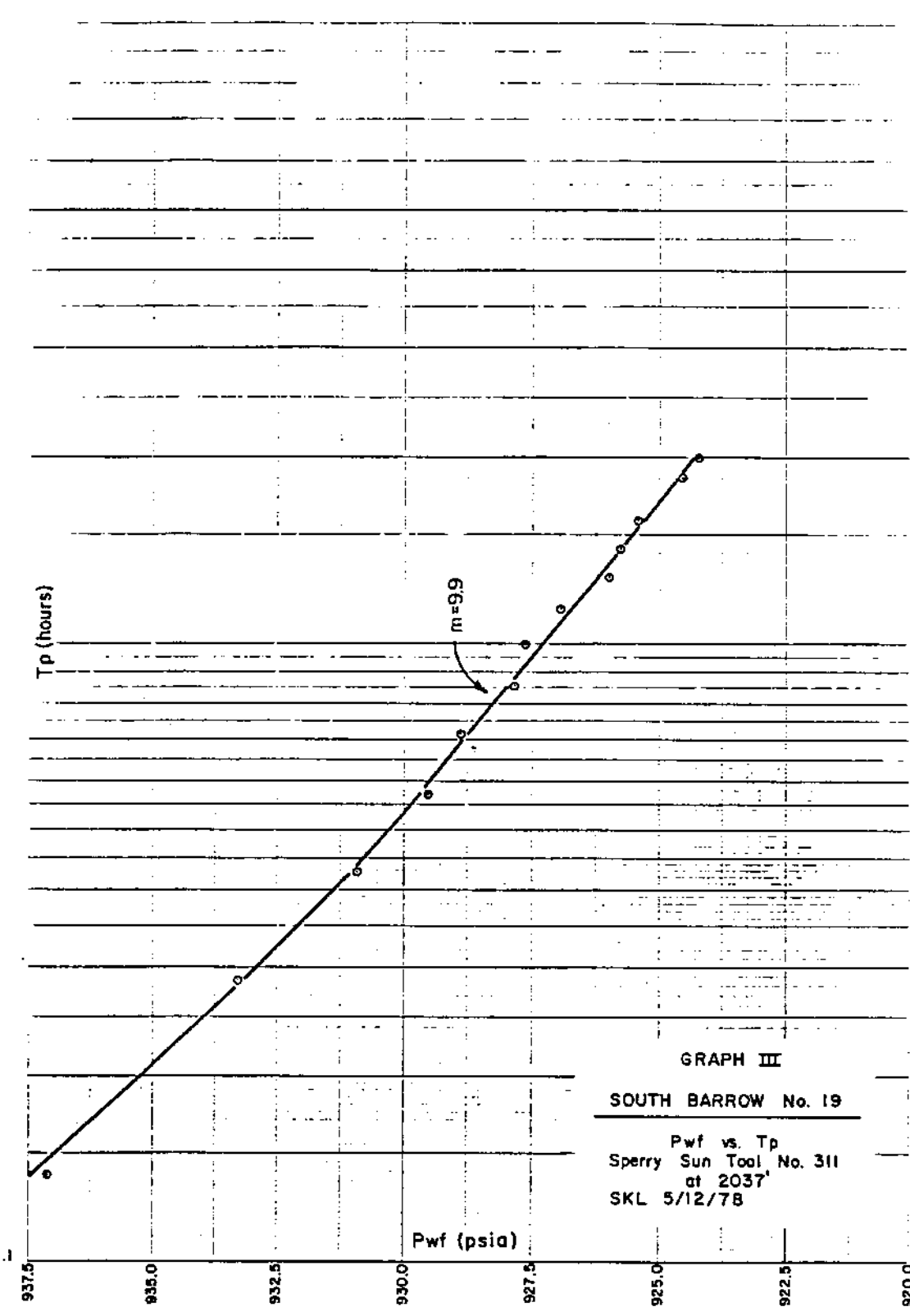
<u>Rate</u>	<u>Choke</u>	<u>Pressure</u>	<u>Flow Rate</u>	<u><math>\Delta P^2</math></u>
1	16/64	924.2 psia	1.170 M <sup>2</sup> cF/d	114077
2	22/64	858.5 psia	2.188 M <sup>2</sup> cF/d	231233
3	26/64	779.4 psia	3.191 M <sup>2</sup> cF/d	360826
4	29/64	724.5 psia	3.687 M <sup>2</sup> cF/d	445165

$$AOF = 7.220 \text{ M}^2\text{cF/d}$$

$$n = .844$$

$$c = .000064062 \frac{\text{M}^2\text{cF/d}}{\text{ps}^2}$$

ATTACHMENT 4



GRAPH III  
 SOUTH BARROW No. 19  
 Pwf vs. Tp  
 Sperry Sun Tool No. 311  
 at 2037'  
 SKL 5/12/78

EXAMPLE CALCULATION III

First Drawdown - Sperry Sun Tool 311 at 2037'

$$I. \quad B_g = Z T \frac{P_{sc}}{T_{sc}} \frac{P_{sc}}{P_i - P_{wf}} \quad T_c = 336.1^\circ R \quad T_R = 1.568$$

$$P_c = 650.9 \quad P_R = \frac{954.1}{650.9} = 1.466$$

$$z = .882$$

$$B_g = .882 \frac{527}{520} \frac{14.65}{954.1} = .01372$$

$$II. \quad \mu_g = \mu_g/\mu_i = 0.0106 \times 1.14 = .012084$$

$$III. \quad C_c = S_g C_g + S_w C_w + CF = (.518 \times .00115225) + (.482 \times 3.3 \times 10^{-6}) + (3.3 \times 10^{-6}) = C_c = .0006017561$$

$$IV. \quad kh = \frac{28984 q \mu_g B_g}{m} \quad q = 1170 \text{ McF/d}$$

$$= 567.9 \text{ mdft} \quad m = 9.9$$

$$k = 35.49 \text{ md} \quad h = 16$$

$$P_{lhr} = 927.3 \text{ psia}$$

$$P_i = 984 \text{ psia}$$

$$r_w = 4.25''$$

$$\phi = .208$$

$$V. \quad S = 1.1513 \left( \left( \frac{P_i - P_{lhr}}{m} \right) - \log \left( \frac{k}{\phi \mu C_{tr} r_w^2} \right) + 3.2275 \right)$$

$$S = .786117$$

$$VI. \quad \Delta P_a = m \times .87(S) = 9.9 \times .87 (.786117)$$

$$= 6.77 \text{ psi}$$

VII. Productivity Index = J

$$J_a = \frac{q}{P_i - P_{wf}} = \frac{1170}{984.0 - 924.2} = 19.57 \frac{\text{McF/d}}{\text{psi}}$$

$$J_i = \frac{q}{(P_i - P_{wf}) - \Delta P_a} = \frac{1170}{984 - 924.2 - 6.77} = 22.06 \frac{\text{McF/d}}{\text{psi}}$$

$$\text{Flow Efficiency} = \frac{J_a}{J_i} = \frac{19.57}{22.06} = .8871$$

ATTACHMENT 6

VIII. Average Gas Mobility = M

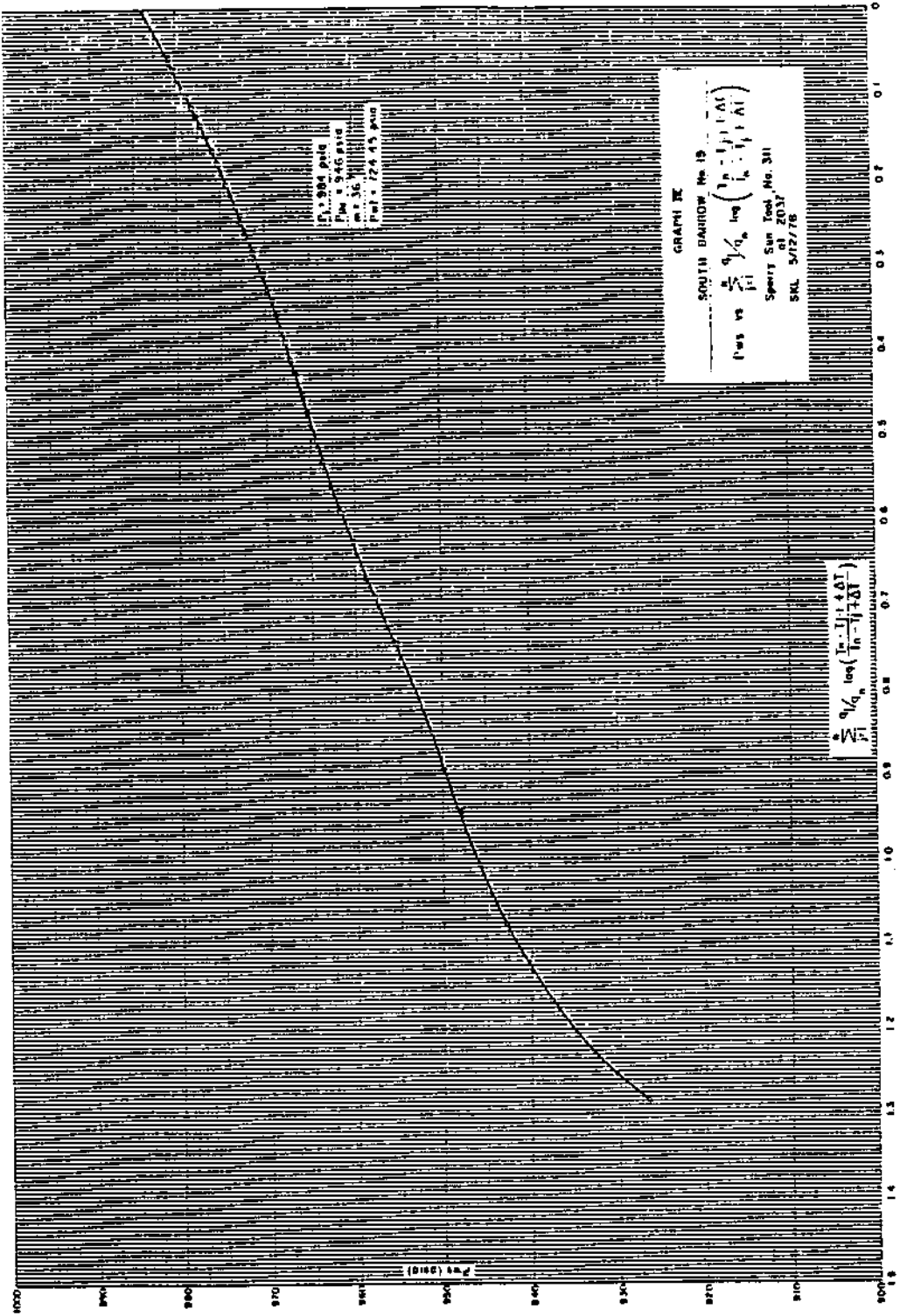
$$M = \frac{k_g}{\mu_g} = \frac{35.49}{.012084} = \frac{2936.94 \text{ md/CP}}$$

IX. Effective Wellbore Radius =  $r_w'$

$$r_w' = r_w e^{-S} = 1.936 \text{ inches}$$

X. Approximate Radius of Investigation =  $r_{inv}$

$$r_{inv} = \sqrt{\frac{0.00105 k T_p'}{\phi \mu C_t}} = 222 \text{ ft}$$



EXAMPLE CALCULATION IV

Final Buildup - Sperry Sun Tool 311 at 2037'

$$I. \quad B_g = Z \frac{T}{T_{sc}} \frac{P_{sc}}{P_i - P_{wf}} \quad T_c = 336.1^{\circ}R \quad T_R = 1.568$$

$$P_c = 650.9 \quad P_R = \frac{854.225}{650.9}$$

$$= 1.312$$

$$Z = .890$$

$$B_g = .890 \frac{527}{520} \frac{14.65}{854.225} = .015469$$

$$II. \quad \mu_g = \mu_i \times \mu_g/\mu_i = .0106 \times 1.12 = .011872$$

$$III. \quad C_t = S_g C_g + S_w C_w + C_F = (.518 \times .00129052) + (.482 \times 3.3 \times 10^{-6}) + (3.3 \times 10^{-6}) = C_t = .0005606721$$

$$IV. \quad kh = \frac{28984}{m} q \mu_g B_g \quad q = 3667 \text{ McF/d}$$

$$m = 36$$

$$h = 16$$

$$P_{1hr} = 946$$

$$P_{wf} = 724.45$$

$$r_w = 4.25''$$

$$\phi = .208$$

$$V. \quad S = 1.1513 \left( \left( \frac{P_{1hr} - P_{wf}}{m} \right) - \log \left( \frac{k}{\phi \mu C_t r_w^2} \right) + 3.2275 \right)$$

$$S = 1.348$$

$$VI. \quad \Delta P_s = m \times .87(S) = 36 \times .87 (1.348)$$

$$= 42.22 \text{ psi}$$

VII. Productivity Index = J

$$J_a = \frac{q}{P_i - P_{wf}} = \frac{3667}{984 - 724.45} = 14.128 \frac{\text{McF/d}}{\text{psi}}$$

$$J_i = \frac{q}{P_i - P_{wf} - \Delta P_s} = \frac{3667}{(984 - 724.45) - 42.22} = 16.873 \frac{\text{McF/d}}{\text{psi}}$$

$$\text{Flow Efficiency} = \frac{J_a}{J_i} = \frac{14.128}{16.873} = 0.837$$

ATTACHMENT 8

VIII. Average Gas Mobility = M

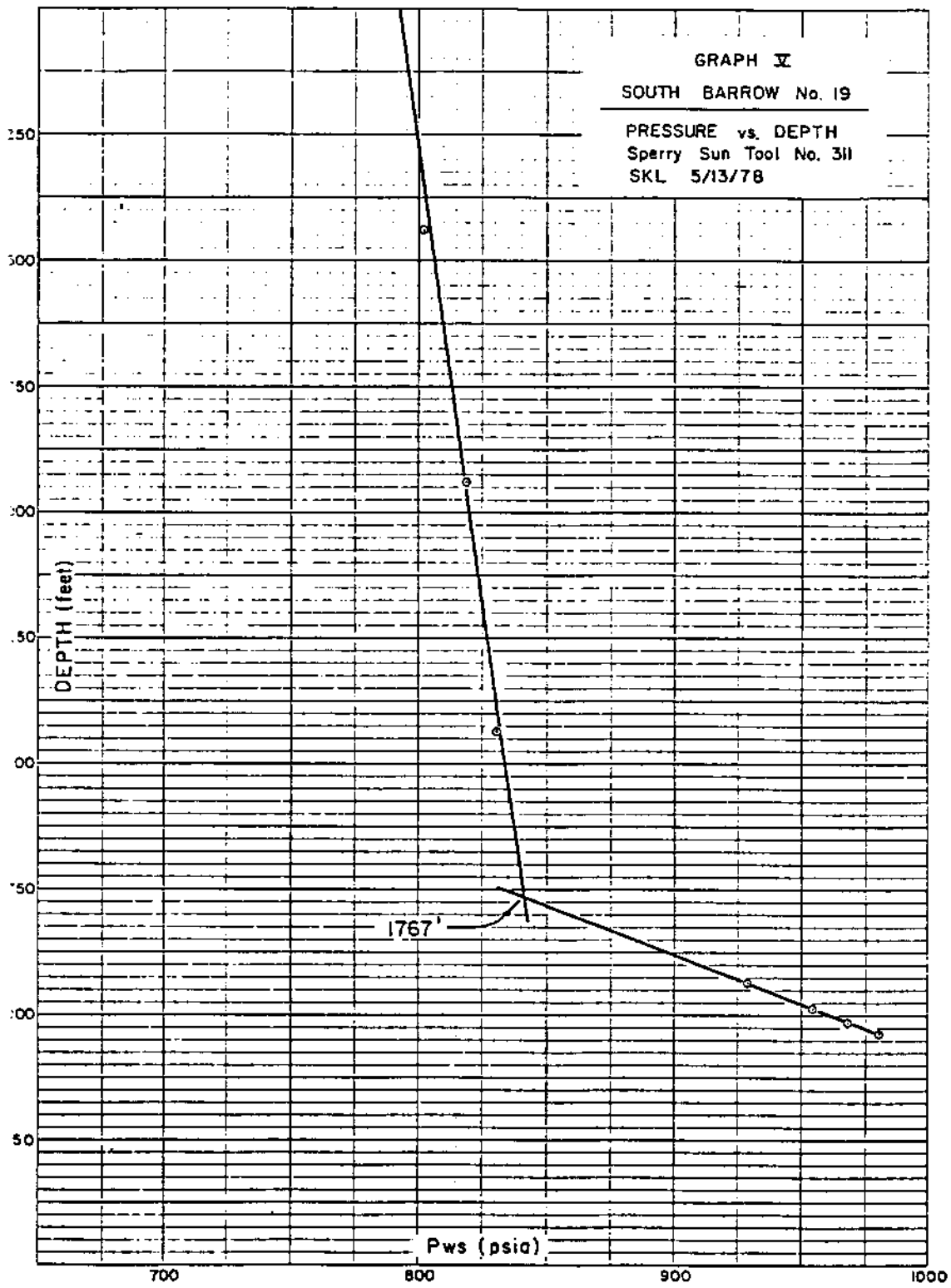
$$M = \frac{k_g}{\mu_g} = \frac{33.89}{.011872} = 2854.6 \text{ md/CP}$$

IX. Effective Wellbore Radius =  $r_w'$

$$r_w' = r_w e^{-s} = 1.104 \text{ inches}$$

X. Approximate Radius of Investigation =  $r_{inv}$

$$r_{inv} = \sqrt{\frac{0.00105 k T_p}{\phi \mu C_t}} = 463 \text{ ft}$$



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EXAMPLE CALCULATION V

Pressure Gradient Test - 5/13/78

<u>D</u>	<u>L</u>	<u>P</u>	<u>ΔP</u>	<u>Gradient</u>
2037	0	980.9	0	-
2012	25	968.1	12.8	.512 psi/ft
1987	25	954.7	13.4	.536 psi/ft
1937	50	929.4	25.3	.506 psi/ft
1437	500	831.0	98.4	.197 psi/ft
937	500	819.7	11.3	.023 psi/ft
437	500	802.2	17.5	.035 psi/ft
0	437	793.0*	9.2	.021 psi/ft*

\*Extrapolated from plot of P vs D

ATTACHMENT 10